

# **Department of Education**

# The New High School for Medowie

Noise and Vibration Impact Assessment Report

Reference: AC04

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This report takes into account the particular instructions and requirements of our client. It is not intended for and should not be relied upon by any third party and no responsibility is undertaken to any third party.

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# 1. Introduction

This Noise and Vibration Impact Assessment Report has been prepared to support a Review of Environmental Factors (REF) for the proposed New High School for Medowie (the activity). The purpose of the REF is to assess the potential environmental impacts of the activity prescribed by State Environmental Planning Policy (Transport and Infrastructure) 2021 (T&I SEPP) as "development permitted without consent" on land carried out by or on behalf of a public authority under Part 5 of the Environmental Planning and Assessment Act 1979 (EP&A Act).

The activity is to be undertaken pursuant to Chapter 3, Part 3.4, Section 3.37 of the T&I SEPP.

The activity will be carried out at 6 Abundance Street, Medowie (the site). The purpose of this report is to:

- Identify noise-sensitive receivers affected by operation and construction of the school
- Set noise and vibration criteria based on relevant standards
- Establish current ambient and background noise levels at and around the site
- Quantify the main sources of construction noise and vibration
- Assess the main operational noise sources, including building services and traffic.
- Determine if criteria are met and recommend mitigation measures if needed.

The assessment evaluates noise and vibration impacts on the surrounding community and land uses, as well as noise intrusion on the proposed school, or activity.

## 1.1 Site description

The site has a street address of 6 Abundance Road, Medowie. It is 6.51ha in area, and comprises 1 allotment, legally described as Lot 3 in DP788451.

A large proportion of the site is currently unused and vacant. A small shed structure and caravan are located adjacent to the northern boundary. A cluster of buildings including a single storey dwelling, an outhouse/shed structure and temporary greenhouse are located within the south eastern corner.

The site contains a largely vegetated area to the south west corner. The site is relatively flat with a gradual fall from west to east toward Abundance Road.

The site has a primary frontage to Abundance Road to the east and Ferodale Road to the north. Abundance Road and Ferodale Road are both classified Local Roads. Medowie Road, approximately 1km east of the site, is a classified Regional Road.

The area surrounding the site mostly consists of industrial, rural residential, educational, and agricultural lands. Adjacent to the north western boundary is a Shell petrol station and mechanic garage. Adjacent to the north eastern boundary is a medical health clinic. Across Abundance Road along the eastern boundary are a number of warehouse and light industrial developments. Directly north of the site across Ferodale Road are large lots used for agricultural purposes. Medowie Public School is located on Ferodale Road, to the north west of the site, opposite the Shell petrol station.

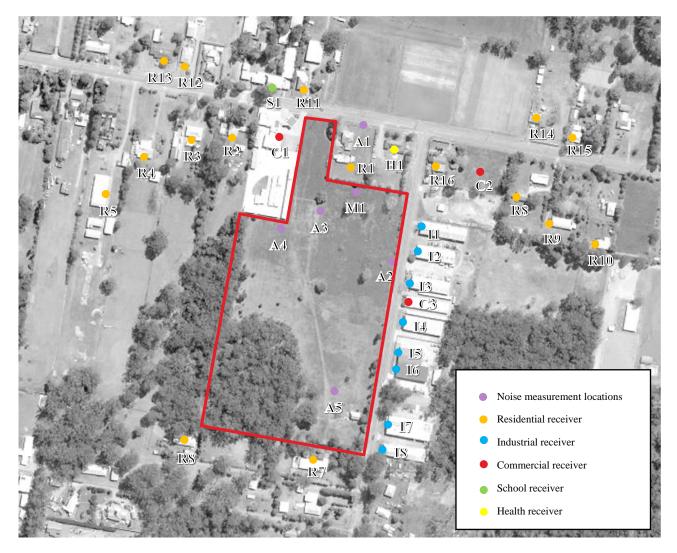


Figure 1: Aerial image of the site including site measurement and sensitive receiver locations

Figure 2 summarises NSW Planning Portal zone classifications for surrounding land uses.



Figure 2: NSW Planning Portal zone classifications

The nearest potentially affected noise sensitive receivers to the site are summarised in Table 1.

Table 1: Nearest noise sensitive receivers

Receiver ID	Address	Classification
R1	28 Ferodale Road, Medowie	Residential
R2	34 Ferodale Road, Medowie	Residential
R3	20 Ferodale Road, Medowie	Residential
R4	18 Ferodale Road, Medowie	Residential
R5	16 Ferodale Road, Medowie	Residential
R6	8A Abundance Road, Medowie	Residential
R7	8 Abundance Road, Medowie	Residential
R8, R9	30A Ferodale Road, Medowie	Residential
R10	32 Ferodale Road, Medowie	Residential
R11	17 Ferodale Road, Medowie	Residential
R12	13 Ferodale Road, Medowie	Residential
R13	11 Ferodale Road, Medowie	Residential
R14	23 Ferodale Road, Medowie	Residential
R15	25 Ferodale Road, Medowie	Residential
R16	30 Ferodale Road, Medowie	Residential
S1	15 Ferodale Road, Medowie	School
Н1	28A Ferodale Road, Medowie	Healthcare
II	5 Abundance Road, Medowie	Industrial
I2	7 Abundance Road, Medowie	Industrial
I3	9 Abundance Road, Medowie	Industrial
I4	13 Abundance Road, Medowie	Industrial
15	15 Abundance Road, Medowie	Industrial
I6	17 Abundance Road, Medowie	Industrial
I7	19 Abundance Road, Medowie	Industrial
18	21 Abundance Road, Medowie	Industrial
Cl	26 Ferodale Road, Medowie	Commercial
C2	30B Ferodale Road, Medowie	Commercial
C3	11 Abundance Road, Medowie	Commercial

## 1.2 Project description

The proposed activity involves the construction of school facilities on the site for the purpose of the New High School for Medowie. The site contains a densely vegetated area to the southwest corner which is identified as land with high biodiversity values corresponding to the areas of remnant native vegetation (PCT 3995 – Hunter Coast Paperbark-Swamp Mahogany Forest). The existing dwelling house and other structures on the site will be demolished as part of the works. No other works are proposed within this area.

The proposed new school will accommodate 640 students in 29 permanent teaching spaces including 3 support teaching spaces across 3-storeys of buildings on the site. The proposed activity be delivered across 1 stage, and will consist of the following:

29 permanent teaching spaces including 3 support teaching spaces, to accommodate 640 students, and school hall to accommodate 1,000 students. Approximately 10,500 sqm of GFA is proposed.

- Main vehicular ingress and egress to Ferodale Road to the north, with a new pedestrian and vehicle crossing proposed.
- Main pedestrian access to Abundance Road.
- Kiss and ride, and bus drop and pick up areas to Abundance Road (6 x parallel spaces).
- New pedestrian wombat crossing to Abundance Road
- Approximately 55 x car parking spaces and 3 x accessible car parking spaces.
- Approximately 70 x bicycle parking spaces.
- Block A (Admin) consisting of administration and learning spaces.
- Block B (Foodtech/Workshop) consisting of food technology rooms and workshops.
- Block C (Hall) consisting of school hall to accommodate 1,000 students.
- Central quad, 1 playing field, and 1 sports courtyard.

The proposed school development will include the following spaces; general learning spaces, General support learning spaces, administrative services, staff areas, gym and canteen, library areas for science, wood and metal, food and textiles, health PE, performing arts, additional learning spaces, student amenities, storage, movement (stairs and covered walkways).

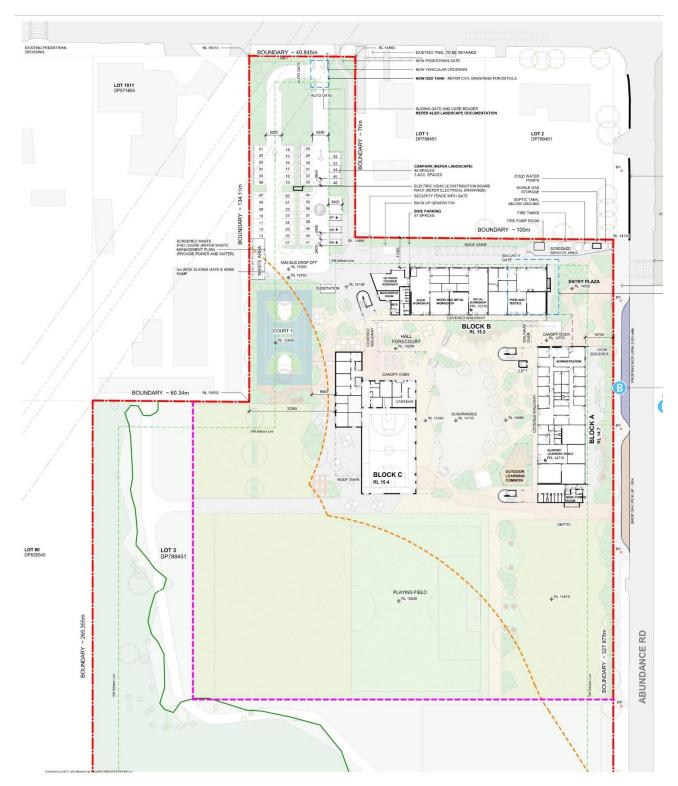


Figure 3: Site Plan - NBRS

# 1.3 Existing acoustic environment

The ambient noise environment observed on site is a combination of significant traffic flows along Abundance and Ferodale Roads, some industrial noise from premises across Abundance Road, idling farm equipment from across Ferodale Road and occasional aircraft movements associated with RAAF Williamtown.

Fact Sheet B of the NSW EPA Noise Policy for Industry (NPI) outlines two methods for determining the background noise level of an area, being 'B1 – Determining background noise using long-term noise

measurements' and 'B2 – Determining background noise using short-term noise measurements'. This assessment has used a combination of long-term and short-term noise monitoring. Measurement locations are depicted in Figure 1.

Unattended measurements were recorded between the  $10^{th}$  and  $18^{th}$  of September 2024. Table 2 presents the overall single Rating Background Levels (RBL) and representative ambient  $L_{Aeq}$  noise levels for each assessment period, determined in accordance with the NPI.

Table 2: Long-term noise monitoring results

Location	Time period <sup>1</sup>	Rating background dBL <sub>A90</sub>	noise levels,	Ambient dBL <sub>Aeq</sub> noise levels			
		Representative Weekday	Representative Week	Representative Weekday	Representative Week		
Logger location M1	Day	41	40	53	53		
IVII	Evening	33	33	48	48		
	Night	29 <sup>2</sup>	29 <sup>2</sup>	47	46		

#### Notes:

1. Day: 07:00-18:00 Monday to Saturday and 08:00-18:00 Sundays & Public Holidays

Evening: 18:00-22:00 Monday to Sunday & Public Holidays

Night: 22:00-07:00 Monday to Saturday and 22:00-08:00 Sundays & Public Holidays

2. Minimum taken to be 30 dBA as per the NPI.

As required by the NPI, the external ambient noise levels presented are free-field noise levels. [i.e., no façade reflection]

The unattended noise monitoring location was selected as being most representative of the site and surrounds while taking into account access, safety and security. Supplementary attended noise monitoring was also conducted on the  $10^{th}$  and  $19^{th}$  of September 2024. Table 3 presents the measured  $L_{Aeq}$  spectrum at each monitoring location.

Table 3: Short term noise monitoring results

Measurement location	Index	Overall dB(A)	Octave	Octave band centre frequency – Hz (dBZ)  Site observations						Site observations	
			63	125	250	500	1k	2k	4k	8k	
A1 – 2 m from Abundance Road	L <sub>eq</sub> , 15min	60	63	60	55	54	57	52	51	46	Dominant source is road traffic (mostly utes and 4wds) on Ferodale Road. Intermittent aircraft mixed
	L90, 15min	42	50	44	37	33	35	31	25	18	with birdsong, idling machinery from farm across road (47 dBA), and busses at Ferodale and Abundance Road intersection (56 dBA).
A2 – 3.5 m from Ferodale Road	L <sub>eq, 15min</sub>	62	63	59	55	57	59	55	49	45	Dominant sources are road traffic on Abundance Road including breaking and acceleration, and industrial sources from warehouses on the opposite side of Abundance Road
	L90, 15min	40	48	40	34	34	35	31	28	21	including fairly consistent drilling/grinding inside the warehouses. Intermittent motorbike/lawnmower revving (60 dBA) and operation around driveway (56 dBA), and delivery truck.
A3 – Approximate location of Hall on site	Leq, 15min	47	57	56	43	36	42	39	35	30	Dominant sources are road traffic on Abundance Road and fairly consistent industrial sources from warehouses on the opposite side of Abundance Road. Intermittent aircraft (52 dBA), birdsong, humming noise and whirley bird from shed behind petrol station, revving of vehicles in warehouses to east (56 dBA) and sound of dogs barking to south.
	L90, 15min	43	50	46	36	32	38	33	29	21	

Measurement location	Index	Overall dB(A)	Octave band centre frequency – Hz (dBZ)  Site observations						Site observations		
			63	125	250	500	1k	2k	4k	8k	
A4 – Western site of boundary adjacent to Petrol Station	Leq, 15min	48	58	55	43	38	41	43	38	28	Dominant sources are road traffic on Abundance Road and fairly consistent industrial sources from
Sallon	L90, 15min	43	52	46	36	32	37	34	29	21	warehouses on the opposite side of Abundance Road. Intermittent aircraft (53dBA) audible from northwest to south of site.  Intermittent noise from sheds south of petrol station, not as loud as other sources to east. Intermittent sound of metal dragged on concrete, banging and clanging (66 dBA) and grinding (59 dBA) from warehouses to east.
A5 - Southern site boundary	Leq, 15min	50	60	55	48	45	46	42	37	31	Dominant source is road traffic on Abundance Road. Intermittent wind
	L90, 15min	46	51	47	40	41	41	37	31	23	in trees, trucks manoeuvring on industrial site across Abundance Road, birdsong, dogs barking and faint airplanes.
M1 - Unattended noise logger	Leq, 15min	50	60	55	47	43	44	42	41	34	Dominant sources are road traffic on Abundance Road and Ferodale Road
location	L90, 15min	43	49	46	38	36	38	34	27	20	predominantly from the west. Intermittent birdsong, distant bang from industrial warehouses across Abundance Road (less than 60 dBA), faint hammering from petrol station, leaves in wind, and horse galloping.

# 2. Acoustic assessment criteria

## 2.1 Relevant standards, guidelines and regulations

The following have been used to develop the noise and vibration criteria for the project:

#### **Local Council Guidelines and Policies**

• Port Stephens Council – Development Control Plan (2024)

#### **NSW Government Guidelines and Policies**

- NSW Department of Education Educational Facilities Standards and Guidelines v2.0, 0001c Design Checklist – Acoustics
- NSW Department of Planning, Development Near Rail Corridors and Busy Roads Interim Guideline (2008)
- NSW Department of Environment and Conservation, Assessing Vibration: A technical guideline (February 2006)
- NSW Environmental Protection Authority Noise Policy for Industry (October 2017)
- NSW State Environmental Planning Policy (Infrastructure) 2007
- NSW Road Noise Policy (March 2011)
- NSW EPA, Environmental Criteria for Road Traffic Noise (1999) Australian and International Standards
- NSW Department of Environment and Climate Change (DECC) "Interim Construction Noise Guideline" (ICNG) 2009.
- NSW Department of Environment and Conservation (DEC) "Assessing Vibration: A Technical Guideline" (AVTG) 2006.
- NSW Protection of the Environmental Operations (POEO) Act 1997.

#### **National Standards**

- AS 2107:2016 Acoustics—Recommended design sound levels and reverberation times for building interiors
- AS 2021:2021 Acoustics Aircraft noise intrusion building siting and construction.
- AS 2436:2010 Guide to Noise and Vibration Control on Construction, Demolition & Maintenance Sites.
- AS 1055:1997 Acoustics Description and Measurement of Environment Noise.

#### **Industry guidelines**

- Association of Australasian Acoustical Consultants (AAAC) Guideline for Educational Facilities, Version 2.0
- Association of Australian Acoustical Consultants (AAAC) Guidelines for Child Care Centre Acoustic Assessment, V 3.0

#### **Sustainability Standards**

• Green Building Council of Australia – Buildings v1

# 2.2 Port Stephens Council DCP

Port Stephens Council Development Control Plan (16 July 2024) summarises assessment requirements for developments within its jurisdiction. Table 4 summarises relevant acoustic assessment requirements.

Table 4: Port Stephens Council Development Controls – Noise and vibration

<b>Development control</b>	Assessment requirements					
B3.2	An acoustic report is required for development that has the potential to produce offensive noise, meaning:					
	• that, by reason of its level, nature, character or quality or the time at which it is made, or any other circumstances:					
	- is harmful to (or is likely to be harmful) to a person who is outside the premises from which it is emitted, or					
	- interferes unreasonably with (or is likely to interfere unreasonably with) the comfort or repose of a person who is outside the premises from which it is emitted					
	• that is of a level, nature, character or quality prescribed by the regulations or that is made at a time, or in other circumstances, prescribed by the regulations, such as the Environmental Protection Authority. 2000, 'NSW Industrial Noise Policy'					
	Note: Development that is likely to require compliance with this requirements includes:					
	• clubs, hotels and pubs with outdoor smoking, dining and gaming areas, mechanical plant, carparks;					
	function centres that host outdoor weddings;					
	• childcare centres with outdoor and indoor play areas, air-conditioning plant, carparks;					
	• residential developments with ventilation and air-conditioning plant, carparks; and					
	• commercial developments with workshops, mechanical and ventilation plant such as air exhaust and supply fans, chillers, cooling towers, truck and freight train movements, loading docks etc.					
B6.1	When development is located within the 2025 ANEF, which is identified by Figure BP, it is classified into one of the following classifications through referencing Figure BL:					
	Acceptable – no design measures required to reduce aircraft noise, or					
	• Conditionally acceptable – design measures required, or					
	- An acoustic report is required for the following:					
	- to support development that is classified as conditionally acceptable					
	- to support subdivision of land and subsequent permissible development types by referencing Figure BL and Figure BM					
	• Unacceptable – development is generally unacceptable. However, details submitted with a development application that demonstrate the following will be considered on a merit-based approach:					
	- Development on a vacant pre-existing lot within the ANEF 25-30 noise contours that satisfies AS 2021 - Acoustics - Aircraft noise intrusion - Building siting and construction indoor noise requirements20					
	- Replacement of a pre-existing dwelling in any of the ANEF noise contours satisfies the AS 2021 - Acoustics - Aircraft noise intrusion - Building siting and construction indoor noise requirements20					
	- Development on land zoned B7 Business Park and adjacent to the Williamtown (Newcastle) Airport					
	Note: Part D15 - Defence or Airport Related Employment Zone (DAREZ) provides site specific requirements for land zoned B7 Business Park and adjacent to the Williamtown Airport					

# 2.3 Operational noise emissions

Consideration is given to the following:

- Noise emission from building services
- Noise emission from school activities and operations; and
- Noise emission from additional traffic generated by the development.

The following sections summarise corresponding assessment criteria.

# 2.3.1 Building services

#### 2.3.1.1 Normal operations

Building services noise emissions is assessed in accordance with the NSW Noise Policy for Industry (NPI) which is primarily concerned with controlling intrusive noise impacts in the short-term for residences and maintaining long-term noise level amenity for residences and other land uses.

The NPI sets out the procedure to determine the project noise trigger for industrial noise sources (e.g. building services equipment). The project noise trigger level is a level that, if exceeded would indicate a potential noise impact on the community and so 'trigger' a management response.

#### Intrusive noise trigger level

The intrusiveness noise trigger level is applicable to residential premises only and is summarised as follows:

LAeq,15minute ≤ Rating Background Level (RBL) plus 5 dB
 (where LAeq,15minute represent the equivalent continuous noise level of the source)

Note that as the Intrusive Noise Trigger Level is established from the prevailing background noise levels at the residential receiver location, the existing background noise level is to be measured.

#### Recommended and project amenity noise level

To limit continuing increases in noise levels from application of the intrusiveness level alone, the ambient noise level within an area from all industrial noise sources combined should remain below the recommended amenity noise levels specified in Table 2.2 of the NPI where feasible and reasonable. An extract from the policy is given below in Table 5.

Table 5: NPI Recommended Amenity Noise Levels (RANLs)

Receiver	Noise amenity area	Time of Day	Recommended amenity noise levels (RANLs) L <sub>Aeq</sub> , dB(A)
Residential	Rural	Day	50
		Evening	45
		Night	40
	Suburban	Day	55
		Evening	45
		Night	40
	Urban	Day	60
		Evening	50
		Night	45
Hotels, motels, caretakers' quarters, holiday	See column 4	See column 4	5 dB(A) above the recommended amenity noise level for a residence for the

Receiver	Noise amenity area	Time of Day	Recommended amenity noise levels (RANLs) L <sub>Aeq</sub> , dB(A)
accommodation, permanent resident caravan parks			relevant noise amenity area and time of day
School classroom - internal	All	Noisiest 1-hour period when in use	35 (see notes for table)
Hospital ward –			
Internal	All	Noisiest 1-hour	35
External	All	Noisiest 1-hour	50
Place of worship –			
Internal	All	When in use	40
Area specifically reserved for passive recreation (e.g. national park)	All	When in use	50
Active recreation area (e.g. school playground, gold course)	All	When in use	55
Commercial premises	All	When in use	65
Industrial premises	All	When in use	70
Industrial interface (applicable only to residential noise amenity areas)	All	All	Add 5 dB(A) to recommended noise amenity area

#### Notes:

The recommended amenity noise levels (RANLs) refer only to noise from industrial sources. However, they refer to noise from all such sources at the receiver location, and not only noise due to a specific project under consideration. The levels represent outdoor levels except where otherwise stated.

- 1. The NPI defines day, evening and nighttime periods as:
- Day: the period from 7 am to 6 pm Monday to Saturday; or 8 am to 6 pm on Sundays and Public Holidays.
- Evening: the period from 6 pm to 10 pm.
- Night: the remaining period.

(These periods may be varied where appropriate. In the case where existing schools are affected by noise from existing industrial noise sources, the acceptable  $L_{Aeq}$  noise level may be increased to 40 dB  $L_{Aeq(1hr)}$ )

The NSW Planning Portal classifies existing development around the site as predominantly Rural Landscape and Large Lot Residential, with some General Industrial (refer Figure 2).

The recommended amenity noise levels (RANLs) represent the objective for total industrial noise at a receiver location, whereas the project amenity noise level (PANL) represents the objective for noise from a single development at a receiver location.

To ensure that any new industrial source of noise is within the RANLs for an area, the PANL applies for each new source of industrial noise as follows:

• Project Amenity Noise Level (PANL) = Recommended Amenity Noise Level (RANL) minus 5 dB(A)

To standardise the time periods for the intrusiveness and amenity noise levels, the policy assumes that the  $L_{Aeq,15min}$  will be taken to be equal to the  $L_{Aeq,period} + 3$  decibels (dB),

#### 2.3.1.2 Project specific noise trigger levels

Based on the background and ambient noise monitoring, Table 6 summarises the derived project specific noise levels based on the NPI.

Table 6: NPI Project specific noise levels

Receiver	Time Period	Project Specific Noise Levels – dB L <sub>Aeq, 15min</sub>				
		Intrusive Noise Trigger Levels	Project Amenity Noise Level (PANL)			
Nearest residential receivers	Day	46	51			
	Evening	38	46			
	Night	35	45			
School outdoor areas	When in use	-	55			
School classroom - internal	Noisiest 1 – hour period		40 L <sub>Aeq(1hr)</sub> <sup>1</sup>			
Hospitals - external	Noisiest 1-hour		50			
Commercial premises	When in use		65			
Industrial premises	When in use		70			

#### Notes:

The school is not expected to operate during the night-time period, with the exception of ad hoc events, therefore daytime criterion is taken as the most onerous target on which assessment of noise emission is based.

#### 2.3.1.3 Modifying factors

Table C1 of the NPI sets modifying factor corrections for annoying noise characteristics such as tonality, dominant low frequency, intermittency or irregularity.

When assessing low frequency impacts, an initial screening test is first undertaken by evaluating whether the difference in noise levels in C-weighted and in A-weighted are 15 dB or more at the receivers, which identifies the potential for an unbalanced spectrum in which case further assessment is required.

#### 2.3.1.4 Sleep disturbance

The NSW NPI also recommends criteria for the assessment of potential sleep disturbance, for the period between 10 pm and 7 am. The school is not expected to operate during this time period, therefore potential sleep disturbance is not being considered.

#### 2.3.1.5 Emergency equipment

There are no provisions in NSW legislation for noise impacts associated with emergency plant.

In lieu of relevant criteria, the VIC EPA State Environment Protection Policy (SEPP) No. N-1 states:

Where the noise source under consideration is a standby generator, standby boiler or fire pump, the noise limit shall be increased by 10 dB for a day period and by 5 dB for all other periods.

This is considered an appropriate provision for short and intermittent operation of equipment during testing such as stair pressurisation fans.

<sup>1-</sup>As stated in table 2.2 note in the NPI, in the case where existing schools are affected by noise from existing industrial noise sources, the acceptable  $L_{Aeq}$  noise level may be increased to 40 dB  $L_{Aeq(1hr)}$ .

#### 2.3.2 School activity

There are no specific regulatory policies or guidelines for noise associated with general school activity. Furthermore, the following is noted from NSW Land and Environment Court (LEC) proceeding (Meriden School v Pedavoli, 22 Oct 2009, case NSW LEC 183)

"All noise that emanates from the normal activities at a school is not offensive".

Notwithstanding, assessment of noise impacts from this type of activity is typically made with reference to the Association of Australasian Acoustical Consultants (AAAC) Guideline for Child Care Centre Acoustic Assessment. The Guideline states the following with respect to outdoor activity:

Up to 4 hours (total) per day – If outdoor play is limited to no more than 2 hours in the morning and 2 hours in the afternoon, the contributed Leq,15 minute noise level emitted from the outdoor play shall not exceed the background noise level by more than 10 dB at the assessment location.

The guidance relating to up to 4 hours outdoor play is deemed appropriate in the context of typical high school programme and activity.

The assessment location is defined as the most affected point on or within any residential receiver property boundary. Examples of this location may be:

- 1.5 m above ground level;
- On a balcony at 1.5 m above floor level;
- Outside a window on the ground or higher floors.

The Guideline states the following with respect to indoor play:

The cumulative Leq,15 minute noise emission level resulting from the use and operation of the childcare centre, with the exception of noise emission from outdoor play discussed above, shall not exceed the background noise level by more than 5 dB at the assessment location as defined above. This includes the noise emission resulting from:

- Indoor play;
- Mechanical plant;
- *Drop off and pick up;*
- Other activities/operations (not including outdoor play).

Assessment of school activities will be guided by these noise management levels to assist in operational management of the school, noting they are aspirational criteria and not mandatory requirements.

#### 2.3.3 Road traffic noise

The NSW Road Noise Policy (RNP) includes assessment criteria for existing noise sensitive receivers affected by additional traffic on existing roads generated by land use developments. These criteria are reproduced in Table 7 for reference.

Table 7: Road traffic noise assessment criteria for residential land uses.

Road category	Type of project / land use	Assessment criteria	
		Day (7am–10pm)	Night (10pm–7am)
Freeway / arterial / sub- arterial roads	Existing residences affected by additional traffic on existing freeways/arterial/sub-arterial roads generated by land use developments	60 dB LAeq, (15 hour) (external)	55 LAeq, (9 hour) (external)

Road category	Type of project / land use	Assessment criteria	
		Day (7am–10pm)	Night (10pm–7am)
Local roads	Existing residences affected by additional traffic on existing local roads generated by land use developments	55 LAeq, (1 hour) (external)	50 LAeq, (1 hour) (external)

Where existing traffic noise levels are above the noise assessment criteria, the primary objective is to reduce these through feasible and reasonable measures to meet the assessment criteria. A secondary objective is to protect against excessive decreases in amenity as the result of a project by applying the relative increase criteria.

In assessing feasible and reasonable mitigation measures, an increase of up to 2 dB represents a minor impact that is considered barely perceptible to the average person.

#### 2.4 Noise intrusion

#### 2.4.1 Internal background noise levels

Section 0.03 of the EFSG Acoustic Checklist states the following:

An internal noise level assessment must be carried out for all new buildings to ensure comfortable acoustic conditions for the spaces occupied.

The internal noise levels within the space must meet the limits stipulated in Table 11.06.1 of Section 11.6 Acoustic Performance Guidelines or be within the range stipulated in Table 1 of the AS/NZS 2107:2016 standard. The more stringent of the two should be met.

For normal operations, internal noise levels are to be met cumulatively taking into account the sources discussed in the following sections.

#### 2.4.1.1 Building services noise

Building services are typically the predominant source of background noise within a space. Internal building services noise targets are set at 3 dB below overall internal noise criteria to allow for cumulative compliance once noise intrusion through façade elements is added.

#### 2.4.1.2 Road traffic noise intrusion

In addition, the EFSGs stipulate that road noise shall be assessed in accordance with the requirements of the State Environmental Planning Policy (Infrastructure) 2007 (ISEPP). It is noted that the ISEPP has been repealed and replaced by State Environmental Planning Policy (Transport and Infrastructure) 2021 (T&I SEPP). The T&I SEPP is supported by the Development Near Rail Corridors and Busy Roads – Interim Guideline, which sets the following internal noise criteria for educational facilities:

Table 8: T&I SEPP internal airborne noise criteria.

Receiver type	Time	Airborne noise daytime  L <sub>Aeq,15h</sub>	Airborne noise night time L <sub>Aeq,9h</sub>
Educational Institutions including child care centres	When in use	40	40

Based on the use of the different spaces, lower internal noise levels may be required in line with the EFSG, therefore, the T&I SEPP criteria should be considered as a minimum legislative requirement.

#### 2.4.1.3 Natural ventilation implications

The internal noise criteria are generally achieved through a sealed building. Ideally where natural ventilation is to be provided, the same criteria would also be achieved, particularly for critical spaces, where higher ambient noise levels may otherwise impact on speech intelligibility or unduly impact concentration.

For less critical uses, research has indicated that occupants are willing to accept trade-offs in the ambient noise levels where natural ventilation is provided. The T&I SEPP guideline generally allows for a + 10 dB concession for the 'open windows' condition. It is noted that for teaching and learning spaces this recommendation is based on the ability to close the windows to achieve internal noise targets.

#### 2.4.2 Outdoor areas

The criteria from the T&I SEPP considers the impact of road traffic noise on internal comfort, but does not address external amenity.

The NSW Environmental Criteria for Road Traffic Noise (ECRTN) and the NSW Road Noise Policy (RNP) provide criteria for school playgrounds and childcare outdoor play areas respectively.

Criteria for outdoor learning areas are not provided by any of the relevant policies and guidelines referenced.

The proposed aspirational non-mandatory noise criteria for outdoor areas are presented in Table 9.

Table 9: Aspirational noise criteria for outdoor areas.

Type of space	Assessment Criteria, L <sub>Aeq, 1hr</sub>
Outdoor school playgrounds	55
Outdoor learning areas	50

The above criteria should be aimed for where possible and practical. But they may not be feasible nor necessary to achieve based on the site constraints and the specific uses proposed for the different areas.

#### 2.4.3 Aircraft Noise

Australian Standard AS 2021:2015 Acoustics - Aircraft Noise Intrusion - Building Siting and Construction sets criteria for aircraft noise intrusion. Reference is made to Australian Noise Exposure Forecast (ANEF) contours with the screening criterion for schools being beyond the 20 ANEF contour.

Williamtown RAAF is situated 6 km to the south of the site. The Williamtown RAAF 2025 ANEF map (see Figure 4) shows that Medowie is located outside of the ANEF 20 contour for any of the contours provided for both the aerodrome and weapons range. The location of the school therefore complies with AS2021 and will not be discussed further in this report.

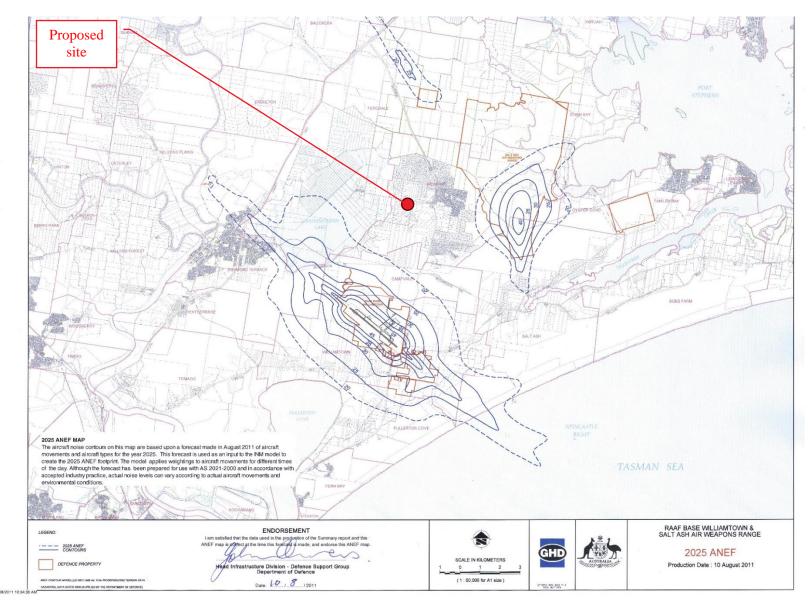


Figure 4: RAAF Base Williamtown Australian Noise Exposure Forecast map 2025

#### 2.5 Construction noise and vibration

#### 2.5.1 Hours of work

Construction works will be undertaken within the hours outlined in Table 10, in accordance with ICNG standard hours of construction

**Table 10: Proposed Hours of Construction** 

Day Standard construction hours	
Monday to Friday	7.00 am to 6:00 pm
Saturdays	8.00 am to 1:00 pm
Sundays or Public Holidays	No construction

In some additional cases, after-hours permits may be sought from the relevant authorities where special requirements exist, for example oversized deliveries.

#### 2.5.2 Construction noise criteria

The Interim Construction Noise Guideline (ICNG) provides recommended noise levels for airborne construction noise at sensitive land uses. The ICNG provides construction management noise levels above which all 'feasible and reasonable' work practices should be applied to minimise the construction noise impact. The ICNG works on the principle of a 'screening' criterion – if predicted or measured construction noise exceeds the ICNG levels then the construction activity must implement all 'feasible and reasonable' work practices to reduce noise levels.

The ICNG sets out management levels for noise at noise sensitive receivers, and how they are to be applied. These noise management levels (NMLs) for residential receivers and other sensitive receivers are reproduced in Table 11 and in Table 12 respectively.

Table 11: Construction noise management levels (NMLs) at residential receivers

Time of day	Management level <sup>1</sup> L <sub>Aeq (15 min)</sub>	How to apply
Recommended standard hours:  Monday to Friday 7am to 6pm Saturday 8am to 1pm No work on Sundays or public holidays	Noise affected RBL + 10dB	The noise affected level represents the point above which there may be some community reaction to noise.  Where the predicted or measured L <sub>Aeq (15 min)</sub> is greater than the noise affected level, the proponent should apply all feasible and reasonable work practices to meet the noise affected level.  The proponent should also inform all potentially impacted residents of the nature of works to be carried out, the expected noise levels and duration, as well as contact details.

Time of day	Management level <sup>1</sup> L <sub>Aeq (15 min)</sub>	How to apply
	Highly noise affected 75dB(A)	The highly noise affected level represents the point above which there may be strong community reaction to noise.
		Where noise is above this level, the relevant authority (consent, determining or regulatory) may require respite periods by restricting the hours that the very noisy activities can occur, taking into account:
		• times identified by the community when they are less sensitive to noise (such as before and after school for works near schools, or mid-morning or mid-afternoon for works near residences
		• if the community is prepared to accept a longer period of construction in exchange for restrictions on construction times.
Outside recommended standard hours	Noise affected RBL + 5dB	A strong justification would typically be required for works outside the recommended standard hours.
		The proponent should apply all feasible and reasonable work practices to meet the noise affected level.
		Where all feasible and reasonable practices have been applied and noise is more than 5dBA above the noise affected level, the proponent should negotiate with the community.
		For guidance on negotiating agreements see section 7.2.2 of the ICNG.

#### Note:

Table 12: Construction noise management levels (NMLs) at other noise sensitive land uses

Land use	Where objective applies	Management level L <sub>Aeq(15 min)</sub> 1
Classrooms at schools and other educational institutions	Internal noise level	45 dB(A)
Hospital wards and operating theatres	Internal noise level	45 dB(A)
Places of worship	Internal noise level	45 dB(A)
Active recreation areas	External noise level	65 dB(A)
Passive recreation areas	External noise level	60 dB(A)
Community centres	Depends on the intended use of the centre.	Refer to the 'maximum' internal levels in AS2107 for specific uses.
Commercial premises	External noise level	70 dB(A)

<sup>1.</sup> Noise levels apply at the property boundary that is most exposed to construction noise, and at a height of 1.5 m above ground level. If the property boundary is more than 30 m from the residence, the location for measuring or predicting noise levels is at the most noise-affected point within 30 m of the residence. Noise levels may be higher at upper floors of the noise affected residence.

Land use	Where objective applies	Management level L <sub>Aeq(15 min)</sub> 1
Industrial premises	External noise level	75 dB(A)
1 - Noise management levels apply when receiver areas are in use only.		

For work within standard construction hours, if after implementing all 'feasible and reasonable' noise levels the site still exceeds the noise affected level, the ICNG does not require any further action – since there is no further scope for noise mitigation.

For out-of-hours work, the ICNG uses a noise level 5 dB below the noise-affected level as a threshold where the proponent should negotiate with the community.

Measured noise data obtained at the logger location most representative of each noise catchment area has been used to derive appropriate noise management levels for the project. These are summarised in Table 4.

**Table 13: Construction Noise Management Criteria for Residential Premises** 

Time Period	Description	NML Criteria L <sub>Aeq (15 min)</sub> 1
During recommended standard hours	Noise affected	51
	Highly noise affected	75
Outside recommended standard hours	Noise affected	46

<sup>1 -</sup> Noise levels apply at the property boundary that is most exposed to construction noise, and at a height of 1.5 m above ground level. If the property boundary is more than 30 m from the residence, the location for measuring or predicting noise levels is at the most noise-affected point within 30 m of the residence.

#### 2.5.3 Construction vibration criteria

#### 2.5.3.1 Disturbance to buildings occupants

Potential vibration disturbance to human occupants of buildings is made in accordance with the NSW Assessing Vibration; a technical guideline. The criteria outlined in the guideline is based on the British Standard BS 6472-1992. Sources of vibration are defined as either 'Continuous', 'Impulsive' or 'Intermittent', as described in Table 14.

Table 14: Types of vibration - Definition

Type of vibration	Definition	Examples
Continuous vibration	Continues uninterrupted for a defined period (usually throughout the day-time and/or night-time)	Machinery, steady road traffic, continuous construction activity (such as tunnel boring machinery).
Impulsive vibration	A rapid build-up to a peak followed by a damped decay that may or may not involve several cycles of vibration (depending on frequency and damping). It can also consist of a sudden application of several cycles at approximately the same amplitude, providing that the duration is short, typically less than 2 seconds	Infrequent: Activities that create up to 3 distinct vibration events in an assessment period, e.g. occasional dropping of heavy equipment, occasional loading and unloading.

Type of vibration	Definition	Examples
Intermittent vibration	Can be defined as interrupted periods of continuous or repeated periods of impulsive vibration that varies significantly in magnitude	Trains, nearby intermittent construction activity, passing heavy vehicles, forging machines, impact pile driving, jack hammers.  Where the number of vibration events in an assessment period is three or fewer, this would be assessed against impulsive
		vibration criteria.

For continuous and intermittent vibration, the preferred and maximum values (in are weighted acceleration values (Wg for z axis and Wd for x and y axes). For intermittent vibration, the preferred and maximum values are Vibration Dose Values (VDVs), based on the weighted acceleration values.

Table 15 reproduces the 'Preferred' and 'Maximum' acceleration values for continuous and impulsive vibration (Wg for z axis and Wd for x and y axes). Table 16 reproduces the 'Preferred' and 'Maximum' Vibration Dose Values (VDVs) for intermittent vibration, based on the weighted acceleration values (Table 2.2 and 2.4 of the Guideline respectively).

Table 15: Preferred and maximum vibration acceleration levels for human comfort, m/s<sup>2</sup>

Location	Assessment	Preferred values		Maximum values	
	period <sup>1</sup>	z-axis <sup>3</sup>	x- and y-axes <sup>3</sup>	z-axis <sup>3</sup>	x- and y-axes <sup>3</sup>
Continuous vibration	n (weighted root-mean	-square (RMS) acceler	ration, m/s <sup>2</sup> , 1-80Hz)	•	•
Critical areas <sup>4</sup>	Day- or night-time	0.0050	0.0036	0.010	0.0072
Residences	Daytime	0.010	0.0071	0.020	0.014
	Night-time	0.007	0.005	0.014	0.010
Offices, schools, educational institutions and places of worship	Day- or night-time	0.020	0.014	0.040	0.028
Workshop	Day- or night-time	0.040	0.029	0.080	0.058
Impulsive vibration	(weighted2 RMS accel	leration, m/s <sup>2</sup> , 1-80Hz)	)	•	•
Critical areas4	Day- or night-time	0.0050	0.0036	0.010	0.0072
Residences	Daytime	0.30	0.21	0.60	0.42
	Night-time	0.10	0.071	0.20	0.14
Offices, schools, educational institutions and places of worship	Day- or night-time	0.64	0.46	1.28	0.92
Workshop	Day- or night-time	0.64	0.46	1.28	0.92

#### Notes:

- 1\_Daytime is 7 am to 10 pm and night-time is 10 pm to 7 am
- 2\_None (to avoid confusion with the acceleration unit)
- 3\_Two frequency weightings (Wg and Wd) are required for the general measurement of whole body vibration with respect to its effect on activities. The weightings should be applied to measurements made in the three vibration axes: Wg for z axis and Wd for x and y axes.

Location	Assessment period <sup>1</sup>	Preferred values	eferred values Maximum values		•	
period		z-axis <sup>3</sup>	x- and y-axes <sup>3</sup>	z-axis <sup>3</sup> x- and y-axes		
4_Examples include hospital operating theatres and precision laboratories where sensitive operations are occurring.						

Table 16: Acceptable vibration dose values (VDV) for intermittent vibration (m/s<sup>1.75</sup>)

Location	Daytime1		Night-time		
	Preferred value	Maximum value	Preferred value	Maximum value	
Critical areas3	0.10	0.20	0.10	0.20	
Residences	0.20	0.40	0.13	0.26	
Offices, schools, educational institutions and places of worship	0.40	0.80	0.40	0.80	
Workshops	0.80	1.60	0.80	1.60	

#### Notes:

- 1\_Daytime is 7 am to 10 pm and night-time is 10 pm to 7 am
- 2\_Note that the VDV is dependent upon the level and duration of the vibration event and the number of vibration events occurring during the assessment period; a higher vibration level is permitted if the total duration of the vibration event(s) is small.
- 3\_Examples include hospital operating theatres and precision laboratories where sensitive operations are occurring. There may be cases where sensitive equipment or delicate tasks require more stringent criteria than the human comfort criteria specified above such as assessing intermittent values against the continuous or impulsive criteria for critical areas and/or referring to criteria in Section 1.2)

#### 2.5.3.2 Impact on structures and services

Potential structural or cosmetic damage to buildings as a result of vibration is typically assessed in accordance with British Standard 7385 Part 2 and/or German Standard DIN4150-3.

#### **Standard structures**

British Standard 7385 Part 1:1990, defines different levels of structural damage as:

Cosmetic – The formation of hairline cracks on drywall surfaces, or the growth of existing cracks in plaster or drywall surfaces; in addition, the formation of hairline cracks in mortar joints of brick/concrete block construction.

Minor – The formation of large cracks or loosening of plaster or drywall surfaces, or cracks through bricks/concrete blocks.

Major – Damage to structural elements of the building, cracks in supporting columns, loosening of joints, splaying of masonry cracks, etc.

BS7385-2 (Table 1 and Section 7.4.2) sets limits for the protection against the different levels of structural damage and those levels (for frequencies within the range 4-250 Hz) are reproduced in Table 17. The criteria relate predominantly to transient vibration that does not give rise to resonant responses in structures, and to low rise buildings.

Where the dynamic loading caused by continuous vibration is such as to give rise to dynamic magnification due to resonance, especially at the lower frequencies where lower guide values apply, the BS7385-2 values may need to be reduced by up to 50%. Activities considered to have the potential to cause dynamic loading in some structures (e.g. residences) include rock breaking/hammering and sheet piling activities. On the basis that the predominant vibration energy occurs at frequencies greater than 4 Hz (and usually in the 10 Hz to 100 Hz range) a conservative vibration damage screening level per receiver type is given below:

Reinforced or framed structures: 25.0 mm/s PCPV

Unreinforced or light framed structures: 7.5 mm/s PCPV

At locations where the predicted and/or measured vibration levels are greater than above, a more detailed analysis of the building structure, vibration source, dominant frequencies and dynamic characteristics of the structure would be required to determine the applicable safe vibration level.

Table 17: BS 7385-2 Structural damage criteria – low rise building

Line	Type of structure	Damage	Damage Peak component particle velocity1 (PCPV), mm/s					
		level	Where vibration that does not give rise to resonant responses in structures <sup>3</sup>			Where vibration might give rise to resonant responses in structures <sup>4</sup>		
		4 Hz to 15 Hz	15 Hz to 40 Hz	40 Hz and above	4 Hz to 15 Hz	15 Hz to 40 Hz	40 Hz and above	
1		Cosmetic	50			25		
	structures Industrial and heavy commercial buildings	Minor2	100			50		
	commercial buildings	Major2	200			100		
2	2 Un-reinforced or light framed structures Residential or light commercial type buildings	Cosmetic	15 to 20	20 to 50	50	7.5 to 10	10 to 25	25
		Minor2	30 to 40	40 to 100	100	15 to 20	20 to 50	50
		Major2	60 to 80	80 to 200	200	30 to 40	40 to 100	100

#### Notes:

#### **Sensitive structures**

German Standard DIN 4150 – Part 3 'Structural vibration in buildings – Effects on Structure' is generally recognised to be conservative and is often referred to for the purpose of assessing structurally sensitive buildings.

Heritage buildings and structures should not be assumed to be more sensitive to vibration unless they are found to be structurally unsound and should otherwise be assessed in accordance with BS7385-2. If a heritage building or structure is found to be structurally unsound (following inspection) DIN 4150-3, line 3 as outlined in Table 18, provides a conservative cosmetic damage objective that should be adopted unless alternative limits are justified by a dilapidation or structural survey. The sensitivity of heritage buildings and other potentially at-risk structures are subject to confirmation by the contractor prior to start of any works.

<sup>1</sup>\_Peak Component Particle Velocity is the maximum Peak particle velocity in any one direction (x, y, z) as measured by a triaxial vibration transducer.

<sup>2</sup>\_Minor and major damage criteria established based on British Standard 7385 Part 2 (1993) Section 7.4.2

<sup>3</sup>\_Levels relates to transient vibrations in low-rise buildings.

<sup>4</sup>\_A 50% reduction might apply to the guide levels for "vibration that does not give rise to resonant responses in structures" if there is potential for continuous vibration to give rise to dynamic magnifications. Activities considered to have the potential to cause dynamic loading in some structures (e.g. residences) include rock breaking/hammering and sheet piling activities.

Table 18: DIN 4150-3 structural damage guideline values

Line	Type of structure	Peak component particle velocity (PCPV), mm/s						
	structure	Vibration at the	foundation at a	At horizontal plane of highest floor	In the vertical direction, at floor slabs			
		1 Hz to 10 Hz	10 Hz to 50 Hz	50 Hz to 100 Hz1	All frequencies	All frequencies		
1	Buildings used for commercial purposes, industrial buildings, and buildings of similar design	20	20 to 40	40 to 50	40	20		
2	Residential buildings and buildings of similar design and/or occupancy	5	5 to 15	15 to 20	15	20		
3	Structures that because of their particular sensitivity to vibration, cannot be classified under lines 1 and 2 and are of great intrinsic value (e.g. listed buildings under a preservation order)3	3	3 to 8	8 to 10	8	202		

#### Notes

#### **Buried services**

DIN 4150-2:2016 part 3 sets out guideline values for vibration effects on buried pipework (see Table 19).

Other services that maybe encountered include electrical cables and telecommunication services such as fibre optic cables. While these may sustain vibration velocity levels from between 50 mm/s and 100 mm/s, the connected services such as transformers and switchgear, may not. Where encountered, site specific vibration assessment in consultation with the utility provider should be carried out.

Table 19: Guideline values for vibration impacts on buried pipework

Line	Pipe material	Peak component particle ve pipe, mm/s	elocity (PCPV) measured on
		Where vibration that does not give rise to resonant responses in structures <sup>3</sup>	Where vibration might give rise to resonant responses in structures <sup>4</sup>
1	Steel, welded	100	50

 $<sup>1\</sup>_At$  frequencies above 100 Hz, the values given in this column may be used as minimum values.

<sup>2</sup>\_Guideline value might have to be lowered to prevent minor damage

Line	Pipe material	Peak component particle velocity (PCPV) measured on pipe, mm/s		
		Where vibration that does not give rise to resonant responses in structures <sup>3</sup>	Where vibration might give rise to resonant responses in structures <sup>4</sup>	
2	Vitrified clay, concrete, reinforced concrete, pre-stressed concrete, metal (with or without flange)	80	40	
3	Masonry, plastic	50	25	
-	High pressure gas pipelines2	75 Monitoring required if predicted above 50. No piling within 15 m of pipeline without detailed assessment.		
-	Electrical cables/Telecommunication services (such as fibre optic cables)	50 to 100 Detailed assessment should be carried out.		

#### Notes:

- 1\_For gas and water supply pipes within 2 m of buildings, the levels given in DIN4150-3 should be applied. Consideration must also be given to pipe junctions with the building structure as potential significant changes in mechanical loads on the pipe must be considered.
- 2\_Based on UK National Grid's specification
- 3\_Levels relates to transient vibrations.
- 4\_A 50% reduction to the guide levels for "vibration that does not give rise to resonant responses in structures" might be appropriate if there is potential for continuous vibration to give rise to dynamic magnifications. Activities considered to have the potential to cause dynamic loading in some structures include rock breaking/hammering and sheet piling activities.

# 3. Operational noise and vibration assessment

# 3.1 Operating Hours

Typical hours of school operations used as the basis of assessment are summarised in Table 20.

Table 20: School hours of operation

Operation	Times
School hours	8am to 4pm, Monday to Friday
Recess and lunch	8am to 4pm, Monday to Friday Various times throughout the day Expected total less than 4 hours
Administration / Office	8am to 4pm, Monday to Friday
Out of hours care	6am to 8am, and 4pm to 6pm Monday to Friday
Vacation care	7am to 6pm, Monday to Friday during school holidays
Gymnasium	6pm to 10pm, Monday to Friday 9am to 10pm, Saturday 9am to 6pm, Sunday
Waste collection	Outside of school hours Monday to Friday

### 3.2 Building services

The preliminary mechanical strategy for the school is expected to be to provide mechanical ventilation and conditioning via the following main items of mechanical plant:

- Condenser units
- Fan coil units; and
- Exhaust fans

Key considerations for mechanical equipment noise mitigation include:

- In the first instance, mitigating noise at the source by opting for low-noise plant selections and operating fans at low-medium speeds should be considered.
- Equipment locations should be nominated to allow reasonable lengths of lined ductwork and duct attenuators where necessary. Locations of externally-located equipment and plantrooms should be reviewed and coordinated with the acoustic consultant.
- The building services design needs to be coordinated to integrate with the architectural design. Room-toroom sound insulation requirements need to be understood in developing air flow strategies, locations
  and detailing of services penetrations through internal partitions and transfer ducts to avoid design
  conflicts.
- Equipment serving rooms with lower noise level criteria such as teaching and learning spaces should be located above a sealed/solid ceiling. If an open or semi-open ceiling is used, fans will likely either need to be located outside the room and ducted in, or 'boxed-out' in a solid plasterboard enclosure.

During ongoing design of the development, equipment will need to be selected and provided with noise and vibration attenuation measures as required to meet the criteria in Section 2.3.1.

A preliminary assessment has been undertaken of key mechanical plant items and has been based on information available at this stage of design and is discussed in the following sections.

#### 3.2.1 Condenser Units

A preliminary layout of Condenser Unit plant rooms and early equipment selections has been developed by the Mechanical Engineers. This information was used to undertake analysis using the ISO 9613 algorithm within the SoundPLAN model developed for the site.

Table 23 summarises the sound power spectrum used as the basis of the mechanical plant noise emission assessment. Lined radiused bend is applied on lower level (L1) and straight lined duct on upper level (L2). On the advice of the mechanical engineer, 75% operation is considered typical.

Table 21: Mechanical plant sound power spectrum - Condenser unit

Equipment	Octave band centre frequency (Hz), Sound power level re: 1pW								
	dB(A)	63	125	250	500	1k	2k	4k	8k
L1 Condenser unit (50 kW) + 50 mm lined radiused bend	67	81	76	70	65	58	55	52	44
L2 Condenser unit (50 kW) + 50 mm lined 1 m straight duct	71	80	80	74	66	58	59	58	51

Appendix B shows grid noise maps of predicted mechanical plant noise emissions to neighbouring receivers.

The predictions demonstrate compliance with target criteria based on the preliminary condenser selections at all nearby noise sensitive receiver locations.

Mechanical plant noise levels in outdoor areas across the school are predicted to be below target criteria for both teaching and learning.

Predicted mechanical noise levels at the nearest affected school facades are more than 10 dB below the prevailing road traffic noise and hence not a driving consideration in façade sound insulation requirements.

Further analysis and refinement of equipment selection and layouts will be necessary during subsequent design stages of design to ensure continued compliance.

#### 3.2.2 Fans

The following preliminary acoustic treatments are recommended for all fans and are based on typical required acoustic treatments. These recommendations will need be reviewed and assessed in detail as the development progresses.

Table 22: Preliminary acoustic mitigation measures - Fans

Equipment	Typical minimum recommended acoustic treatment	
Outside air fans	<ul> <li>Minimum 2 m internally lined duct on each side of fan.</li> <li>External lagging of fan plus flexible connections and 2m of duct on each side of fan.</li> </ul>	
	• For the Gymnasium, allowance for acoustic louvres on intake and attenuators on supply.	
Toilet exhaust fans	Minimum 2 m internally lined duct on each side of fan.     External lagging of fan plus flexible connections and 2m of duct on each side of fan.	

Equipment	Typical minimum recommended acoustic treatment				
Kitchen exhaust fans <sup>1</sup>	Internally lined ductwork on exhaust side of each fan.				
Smoke exhaust fans	Allowances for attenuators on exhaust.				
Dust extraction fan <sup>1</sup>	Allowances for muffler and minimum 2 m lined ductwork on exhaust.				

<sup>&</sup>lt;sup>1</sup> It is understood that Kitchen exhaust and Dust extraction fans are not required to meet EFSG specified internal noise levels.

#### 3.2.2.1 Dust extraction system

A review has been undertaken based on preliminary selections for dust extraction systems associated with the Wood Workshop. Final equipment selection and associated acoustic attenuation will need to be confirm during detailed design.

In the context of the school development and surrounding environment, the dust extraction system must adhere to a maximum sound pressure level of 50 dB(A) at 1 m from the exhaust opening to comply with environmental noise emission criteria.

#### 3.2.3 Fan Coil Units

An acoustic review has been undertaken of preliminary FCU selections and typical arrangements provided by the Mechanical Engineer. A summary of minimum recommended acoustic treatments is provided in Table 23.

**Table 23: Typical FCU acoustic treatments** 

Design criteria	Minimum recommended acoustic treatment					
	Supply/outlet	Return/inlet	Casing			
30 dB(A) Support Learning	1 m of 50 mm internally lined duct + 1.8 m 33% open area attenuator + three 2 m of acoustic flex duct	1.8 m 33% open area attenuator + one 50 mm lined elbow bend into 27 m <sup>3</sup> plenum	Plasterboard boxing OR External lagging + mass loaded vinyl in ceiling to 1m beyond FCU in all directions			
35 dB(A) General Learning	1 m of 50 mm internally lined duct + 1.2 m 33% open area attenuator + three 2 m of acoustic flex duct	1.2 m 33% open area attenuator + one 50 mm lined elbow bend into 27 m³ plenum  OR  1.8 m 27% open area attenuator + one 50 mm lined elbow bend	Plasterboard boxing OR External lagging + mass loaded vinyl in ceiling to 1m beyond FCU in all directions			
35 dB(A) Interview, Private offices, Study <sup>1</sup>	1.2 m 33% open area attenuator + three 1 m of acoustic flex duct	1.5 m 38% open area attenuator + one 50 mm lined elbow bend	Plasterboard boxing OR External lagging + mass loaded vinyl in ceiling to 1m beyond FCU in all directions			
40 dB(A) Library	1 m of 50 mm internally lined duct + 0.9 m 43% open area attenuator + three 1 m of acoustic flex duct	0.9 m 43% open area attenuator + one 50 mm lined elbow bend into room	External lagging			

Design criteria	Minimum recommended acoustic treatment				
	Supply/outlet	Return/inlet	Casing		
40 dB(A) Open Offices, Reception, Staff Areas	1 m of 50 mm internally lined duct + 0.9 m 38% open area attenuator + three 1 m of acoustic flex duct	0.9 m 33% open area attenuator + one 50 mm lined elbow bend into room	External lagging		

#### 3.2.4 Electrical equipment

The 1000kVA substation proposed to the northwest of the site is expected to be readily controlled via standard enclosure.

An emergency generator is proposed at the northern boundary of the site. This generator will require a dedicated acoustic enclosure and treatment to intakes and exhaust flues to meet emergency criteria summarised in Section 2.3.1.5. A preliminary analysis has been undertaken and the acoustic performance in Table 24 with the generator working at full load is expected to be required to meet the criteria. Further detail and revision of this requirement will need to be specified during subsequent stages of design.

Table 24: Preliminary acoustic performance requirements – Standby generator

Item	Sound level description	Leq(1-minute), dB(A)	Leq(1-minute), dB(C)
Generator enclosure – overall	Sound Power	87	91

#### Notes:

Adverse impacts to either the school or nearby noise sensitive receivers is not anticipated provided sufficient attenuation is specified for these items of electrical equipment, the details of which are to be worked through in subsequent phases of design.

#### 3.3 Operational activities

#### 3.3.1 Outdoor play areas

Assessment of noise emission from outdoor play areas is based on the following assumptions:

- Both passive (e.g. courtyard) and active (e.g. sports) outdoor play areas defined in the architectural site plan (refer Figure 3).
- Noise source levels of students playing outdoors determined in accordance with the method outlined in the AAAC Guidelines (refer Table 25).
- Number of students occupying an outdoor play area derived based on expected class sizes and scaled to incorporate a combination of active and passive play.
- Court and sports field are each assessed to have 30 students engaged in active play, and the quadrangle is assessed to have 320 students engaged in active play, and 320 students engaged in passive play. This is considered a conservative approach to assessment.

<sup>&</sup>lt;sup>1</sup> - Noise emission from the acoustic enclosure shall be free of the tonal, modulated and impulsive noise (refer to NSW Industrial Noise Policy).

<sup>&</sup>lt;sup>2</sup> - The total sound power shall be inclusive of the load banks if present.

Table 25: Sound power spectra for outdoor play areas - AAAC

Source	Overall dB(A)	Octave band centre frequency, Hz								
		31.5	63	125	250	500	1k	2k	4k	8k
Active Play (per 10 children)	87	64	70	75	81	83	80	76	72	87
Passive Play (per 10 children)	81	58	64	69	75	77	74	70	66	81

Resultant predicted noise levels from outdoor play activity are summarised in Table 26.

Table 26: Predicted noise levels from outdoor play areas

Receiver	Target criterion – day (dBL <sub>Aeq,15min</sub> )	Predicted noise level (dBL <sub>Aeq,15min</sub> )	Compliance?	
R1	51	47	Yes	
R2	51	33	Yes	
R3	51	33	Yes	
R4	51	32	Yes	
R5	51	31	Yes	
R6	51	38	Yes	
R7	51	42	Yes	
R8	51	39	Yes	
R9	51	35	Yes	
R10	51	31	Yes	
R11	51	41	Yes	
R12	51	31	Yes	
R13	51	31	Yes	
R14	51	30	Yes	
R15	51	30	Yes	
R16	51	44	Yes	
S1	501	40	Yes	
Н1	50	37	Yes	

#### Notes:

 $1-10~\mathrm{dB}$  is added to the façade incident sound pressure level to account an expected minimum  $10~\mathrm{dB}$  attenuation through an open window for the school criteria being an internal noise objective

Noise levels during times when the entire student body is using the outdoor play areas (i.e. recess and lunch) are expected to comply with the operational noise criteria for all residential receivers. This is considered a

worst case and likely infrequent scenario with the entire school population occupying the outdoor quadrangle. During more frequent periods when the outdoor areas are used for structured learning activities, noise levels are expected to be significantly lower.

To help mitigate this potential impact, strategic site planning has been implemented, incorporating buffer zones that increase the distance between major activity areas and nearby receivers. The current design places active play areas away from residential areas and utilizes perimeter buildings to shield much of the noise generated.

#### 3.3.2 Gymnasium noise breakout

Assessment of noise breakout from the Gymnasium has been undertaken based on the following scenarios:

- Noise source: internal reverberant level of up to 75 dBA which considers a typical worst case noisy learning activity / setting from sports and music.
- Windows / doors open this includes bifold glazing doors and high-level louvres for natural ventilation

Table 27 summarises predicted noise levels at the nearest noise sensitive receiver locations due to noise breakout from the Gymnasium.

Table 27: Predicted Gymnasium noise breakout

Receiver	Target criterion (dBL <sub>Aeq,15min</sub> )			Predicted noise lev	Compliance?	
	Day	Evening	Night	Doors open	Doors closed	
R1	46	38	35	29	9	Yes
R2	46	38	35	11	4	Yes
R3	46	38	35	11	4	Yes
R4	46	38	35	17	3	Yes
R5	46	38	35	18	6	Yes
R6	46	38	35	11	5	Yes
R7	46	38	35	32	8	Yes
R8	46	38	35	15	0	Yes
R9	46	38	35	12	0	Yes
R10	46	38	35	11	0	Yes
R11	46	38	35	15	8	Yes
R12	46	38	35	6	0	Yes
R13	46	38	35	5	0	Yes
R14	46	38	35	22	0	Yes
R15	46	38	35	18	0	Yes
R16	46	38	35	32	10	Yes
S1	501	-	-	13	7	Yes
H1	50	•		17	14	Yes

Receiver T	Target criterion (dBL <sub>Aeq,15min</sub> )			Predicted noise lev	Compliance?	
С	Day	Evening	Night	Doors open	Doors closed	

#### Notes:

Predicted noise breakout from typical Gymnasium use are expected to comply with target criteria during all time periods with doors open and doors closed.

#### 3.3.3 Covered outdoor workshop area

Feedback obtained during Technical Stakeholder Group meetings with SINSW representatives identified that the COWA is an area where handheld tools (i.e. circular saws and angle grinders) are occasionally used to process larger deliveries. There is no requirement for this space to meet internal noise level criteria for teaching and learning as it is not a regular function of the space.

Analysis of noise breakout from the Covered Outdoor Workshop Area was investigated using a circular saw as a worst case high noise generating piece of equipment. Analysis was based on the architectural configuration in Figure 5.

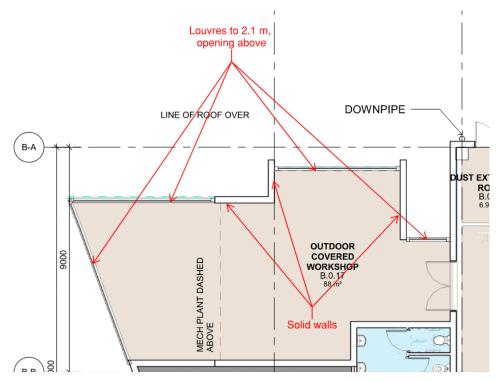


Figure 5: Indicative COWA layout

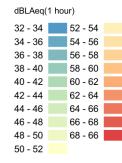
Three scenarios were explored as follows:

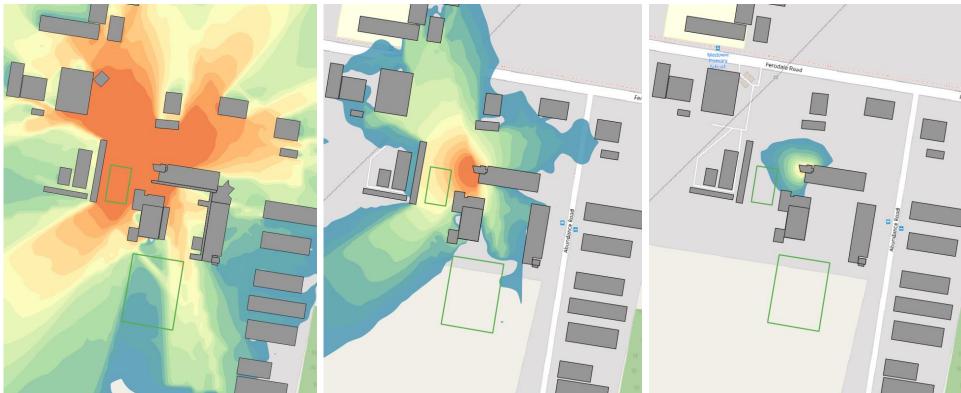
- Weather louvres (full height)
- Acoustic louvres (minimum required for natural ventilation)
- Fully enclosed (mechanical ventilation)

For all scenarios soffit mounted acoustic treatment is incorporated to control reverberant noise build up.

Figure 6 shows predicted noise impact from operation of a circular saw within the COWA with and without acoustic treatment.

 $<sup>1-10~\</sup>mathrm{dB}$  is added to the façade incident sound pressure level to account an expected minimum  $10~\mathrm{dB}$  attenuation through an open window for the school criteria being an internal noise objective





Full height regular louvres

Minimum acoustic louvres for natural ventilation

Fully enclosed facade

Figure 6: Predicted noise breakout from COWA – Circular saw

Predicted noise levels with no acoustic treatment in place are more than 20 dB above the existing ambient background noise at the nearest residential receivers and 60 dBA through the school courtyard.

Inclusion of acoustic louvres brings noise levels at the nearest noise sensitive receiver to within industrial noise emission criteria. All outdoor noise criteria for the school itself also comply with the target criteria with the exception of the basketball court immediately to the west.

It is necessary to fully enclose the COWA to achieve any further mitigation of noise breakout. This approach would result in the space no longer being 'outdoor'.

It is reiterated that this assessment has been conducted on the basis of very noisy equipment being used. Should operational constraints be placed on the space to not incorporate the use of powered machinery, it would be acceptable to retain a weather louvre façade.

#### 3.3.4 Carpark

Assessment of carpark noise impacts to nearby noise sensitive receivers has been made with reference to the AAAC Guidelines. Typical sound power levels for vehicles within the car park area used as the basis of assessment are summarised in Table 28.

Table 28: Typical sound power levels for vehicles within the car park

Vehicle	Level (dBL <sub>Aeq</sub> )
Car	81
Delivery van	86

The latest architectural plans show provision for a 55 space car par with entrance via Ferodale Road. As a conservative worst-case scenario the car park noise assessment has considered the following:

- Noise source locations closest to the affected residences within the car park area.
- Up to 3 vehicle movements over a 15-minute period.

The predicted operational noise levels associated with the car park are summarised in Table 29.

Table 29: Predicted car park operational noise levels

Receiver	Target criterion (dBL <sub>Aeq,15min</sub> )	Predicted noise level (dBL <sub>Aeq,15min</sub> )	Compliance?
R1	46	46	Yes
R2	46	31	Yes
R3	46	30	Yes
R4	46	20	Yes
R5	46	25	Yes
R6	46	22	Yes
R7	46	22	Yes
R8	46	28	Yes
R9	46	26	Yes
R10	46	23	Yes
R11	46	38	Yes

Receiver	Target criterion (dBL <sub>Aeq,15min</sub> )	Predicted noise level (dBL <sub>Aeq,15min</sub> )	Compliance?
R12	46	23	Yes
R13	46	21	Yes
R14	46	23	Yes
R15	46	21	Yes
R16	46	34	Yes
S1	501	36	Yes
Н1	50	24	Yes

#### Notes:

The operational noise levels of the car park are expected to meet target criteria at all locations. The car park will primarily be used during daytime hours and will feature controls, such as gate access, to restrict public and after-hours usage. Speed limits will help reduce noise emissions from vehicles accessing and navigating the car park.

#### 3.3.5 School traffic

The predicted worst-case traffic volumes (i.e busiest 1-hour periods) on the surrounding road network due to the operation of the school is presented in Table 30. This information was provided by WSP on 26 November 2024 and has been used to determine the predicted relative increase in road traffic noise level as a result of the project by analysing against future predicted road traffic numbers summarised in Section 3.4.1.

Table 30: Forecast peak hourly traffic - relative increase

Road	School traffic		
	AM Peak	PM Peak	
Abundance Road	258	194	
Ferodale Road (west of Abundance)	127	99	
Ferodale Road (east of Abundance)	177	135	

Based on the predicted increase in road traffic during peak periods, the road traffic noise levels are not expected to increase by more than the 2 dB screening criterion summarised in Section 2.3.3.

All other times outside of peak times are expected to result in similar noise level to existing conditions due to relatively little road traffic activity from the school during these times.

#### 3.3.6 Public Address

Noise from public address systems has the potential to affect nearby noise sensitive receivers. To reduce the likelihood of noise disturbance to surrounding properties, the following measures are recommended for all public address systems:

• Restrict usage to daytime hours only (7am to 6pm).

 $<sup>1-10~\</sup>mathrm{dB}$  is added to the façade incident sound pressure level result to account for the criteria for schools being an internal noise criteria

- Use best practice design, including directional speakers that focus inward toward the school and cover only the necessary areas.
- Set volume levels to the minimum required to ensure clarity and audibility within the designated coverage zones, as specified in EFSG.

#### 3.3.7 Waste Removal, Deliveries and Cleaning

There will be a limited number of deliveries or waste removals on any given day. To minimize disturbance to nearby residents, it is recommended that all loading dock activities and waste removal take place between 7:00 AM and 10:00 PM.

To prevent disturbing the sleep of nearby residents, it is recommended that all noisy cleaning activities be conducted between 7:00 AM and 10:00 PM. If activities must occur between 10:00 PM and 7:00 AM, the following measures should be taken:

- Ensure windows and doors are closed to minimize noise emissions.
- Do not operate air conditioning.
- Refrain from performing outdoor cleaning activities (e.g., leaf-blowing).

#### 3.4 Noise intrusion

#### 3.4.1 Road Traffic

The primary source of noise intrusion for the site is existing and future projected road traffic on the immediately adjacent road network.

A road traffic noise model has been built using the Calculation of Road Traffic (CoRTN) algorithm in SoundPLAN 9.0 to predict road traffic noise levels throughout the site. This noise model is constructed from the following inputs:

- Terrain mesh extracted from Elvis Elevation and Depth Foundation Spatial Data.
- Existing building structures, digitized from geolocated satellite imagery.
- Proposed school building structures, digitized from supplied drawings by NBRS.
- Surrounding road network strings, digitized from geolocated satellite imagery.
- Road traffic data for Abundance Road and Ferodale Road supplied by WSP.

Road traffic data noise model inputs provided by WSP on 12 September 2024 are summarised in Table 31. Posted speed limits of 60 km/hr were adopted for both Abundance Road and Ferodale Road.

Table 31: Forecast peak hourly traffic

		Ferodale Road (West of Abundance)		Abundance Road		Ferodale Road (East of Abundance)	
		Eastbound	Westbound	Eastbound	Westbound	Eastbound	Westbound
Stage 1 2026							
AM Peak	LV	256	306	203	304	359	510
	HV	7	3	6	11	10	11
PM Peak	LV	320	218	215	232	458	373
	HV	6	1	1	8	4	6
Stage 1 2036							

		Ferodale Road (West of Abundance)		Abundance Road		Ferodale Road (East of Abundance)	
		Eastbound	Westbound	Eastbound	Westbound	Eastbound	Westbound
AM Peak	LV	325	386	247	373	459	646
	HV	10	4	8	15	14	15
PM Peak	LV	407	281	270	287	588	479
	HV	9	1	1	11	6	8
Stage 2 2036							
AM Peak	LV	355	423	301	450	491	708
	HV	10	4	8	15	14	15
PM Peak	LV	442	295	304	339	621	509
	HV	9	1	1	11	6	8

Road traffic noise model and outputs are summarised in Appendix C and have been used as the basis of assessments discussed in Section 3.4.3 and 3.4.4. It is noted that these predicted levels are based on peak hourly flows and are therefore considered to represent the worst case period of the day.

The following measured road traffic noise spectrum has been scaled based on the outputs of the SoundPLAN model to analyse road traffic noise intrusion into the school buildings.

Table 32: Measured road traffic noise spectrum

Measurement	Octave bar	Octave band centre frequency – Hz (dBZ)							
	63	125	250	500	1k	2k	4k	8k	
Measured road traffic noise spectrum	63	60	55	54	57	52	51	46	

#### 3.4.2 Industrial noise

A preliminary noise study was undertaken on 24 April 2024 to determine potential impacts to the proposed school from industrial noise sources across Abundance Road (refer SLR report 630.031480.00001-R01-v0.1-20240424). The assessment found that noise levels of up to 57 dBA could be expected at the worst affected facades of Building B facing Abundance Road. This is in the order of 6 dB less than road traffic noise predictions to this façade. On this basis, specification of façade glazing to mitigate road traffic noise is also expected to address industrial noise intrusion.

#### 3.4.3 Building envelope

#### *3.4.3.1 Glazing*

Table 33 summarises recommended façade glazing to control road traffic noise intrusion to internal spaces based on the predicted noise levels summarised in Appendix C and latest architectural drawings.

It is noted that the quoted performance is not only subject to the glazing selection but also to the construction of the window frame and the frame seal selection.

Table 33: Minimum sound insulation requirements and indicative constructions - Façade glazing

Building	Façade	External Noise Level	Internal Noise Level Criteria	Façade Glazing	
		LAeq, 1hr		Recommended Minimum Sound Insulation Performance Rw+Ctr	Indicative Construction
A	East – Facing Abundance Road	64	30 (SLU, Performing Arts) 35 (General Learning, Interview, Private Offices)	37	12.5 mm laminated glass
			40 (Reception Office, Library, PE Fitness Laboratory)	33	10 mm float glass / 12 mm cavity / 6 mm laminated glass
В	North – Facing Ferodale Road	54-61	35 (General Learning) 40 (Open Office / Staff Lounge, Workshops)	27	6.38 mm laminated glass
			50 (Storeroom, Kitchen, Amenities)	20	Standard 4 mm float glass
A and B	A West and B South – Facing	48-54	30 (Performing Arts)	28	6 mm float glass / 12 mm cavity / 6.38 mm laminated glass
	internal courtyard		30 (SLU, Workshops)	27	6.38 mm laminated glass
			35 (General Learning, Study, Visual Arts, Textile, Interview, Seminar and Private Offices, Staff Lounge)	27	6.38 mm laminated glass
			40 (Reception Office, Library, PE Fitness and Science Laboratories)	20	Standard 4 mm float glass
			50 (Storeroom, Amenities)		
С	South	48-51	30 (Assembly)	27	6.38 mm laminated glass

#### 3.4.3.2 Natural ventilation

The design currently allows for openable windows within General Learning Spaces. Internal noise criteria will not be met with the windows open. Further it is noted that operable windows typically do not perform as well acoustically as fixed glazing. The inclusion of mechanical ventilation should allow for windows to remain closed and the option for sealed glazing to be installed for General Learning Spaces.

A review has been undertaken of natural ventilation openings proposed in the Gymnasium. Natural ventilation louvres are proposed to be located the upper west and east façade of the gymnasium, measuring approximately 26 m long and 1.5 m high.

Analysis of the proposed natural ventilation openings has been made based on road traffic noise levels summarised in Appendix C. Results show that an acoustic louvre will be required to meet internal noise criteria for Assembly Halls.

Table 34 summarises transmission loss spectrum for acoustic louvres used in road traffic noise predictions..

Table 34: Acoustic louvre minimum sound transmission loss

Item	Transmission Loss, dB Octave Band Centre Frequency, Hz			z				
	63	125	250	500	1k	2k	4k	8k
Acoustic louvre	-5	-10	-14	-22	-27	-25	-21	-17

#### 3.4.3.3 External doors

Schools Infrastructure Pattern Book: Standardised Designs for Schools, Volume 2 Building Components provides the following indicative guidance for external entry doors:

Entry doors to occupied teaching, music, drama and sports spaces: Solid core, minimum 35 mm thick with acoustic weather (where external) seals on all rebated closing faces. Gap at floor to be minimized.

In addition to the above requirement, a preliminary review has been undertaken of noise break-in via external doors based on road traffic noise levels summarised in Appendix C. The following guidance is provided:

- All single external facing doors should be minimum R<sub>w</sub> 30 to meet internal noise levels
- $\bullet$  Doors to the wood and metal workshop should be minimum  $R_w$  35 to control noise breakout to courtyard and teaching spaces
- The door between the outdoor workshop (COWA) to internal wood workshop should be R<sub>w</sub> 30
- Gymnasium glazed vertically folding doors should be R<sub>w</sub> 32 to control noise break-in

#### 3.4.3.4 Façade wall

Masonry and concrete façade wall elements are considered sufficient to mitigate road traffic noise intrusion. There is a potential for noise intrusion to be more significant where lightweight wall systems are proposed. Minimum sound insulation requirements and indicative constructions have been developed and are summarised in Table 35.

Table 35: Minimum sound insulation requirements and indicative constructions - Lightweight façade walls

Building	Façade	Minimum sound insulation requirement, R <sub>w+Ctr</sub>	Indicative construction
A and B	North, South and West	40	3 mm aluminium cladding + 6 mm fibre cement + 200 mm timber stud cavity + 100 mm fibreglass insulation + 13 mm plasterboard
A	East – general spaces	45	3 mm aluminium cladding + 6 mm fibre cement + 200 mm timber stud cavity + 100 mm fibreglass insulation + 2 x 13 mm plasterboard
A	East –Performing Arts space	47	3 mm aluminium cladding + 6 mm fibre cement + 200 mm timber stud cavity + 100 mm fibreglass insulation + 2 x 16 mm Fyrchek plasterboard ( or 3 x 13 mm plasterboard)

#### 3.4.4 Outdoor areas

Predicted road traffic noise levels across the site are shown in Appendix C and summarised for outdoor areas in Table 36 against aspirational criteria for outdoor areas presented in Section 2.4.2.

Table 36: Predicted road traffic noise levels - Outdoor Areas

Area	Predicted road traffic noise level dBL <sub>Aeq,1hr</sub>	Complies?	Comments
Quadrangle	48-51	Yes	Within target criteria for outdoor areas.  Under cover areas shielded by Building Positoble for
			by Building B suitable for outdoor learning.
Outdoor sport areas	48-58	Partial	Western half within target criteria for outdoor areas.
			Eastern half up to 3 dB above.
			Inclusion of barrier/berm not considered feasible in the context of proposed school layout.
Covered outdoor workshop area (COWA)	51	Yes	Considered suitable for outdoor teaching and learning, 1 dB exceedance considered negligible.

Area	Predicted road traffic noise level dBL <sub>Aeq,1hr</sub>	Complies?	Comments
Covered outdoor learning area (COLA)	48-54	Partial	Majority of area within target criteria for outdoor learning.
			Southern portion up to 4dB above outdoor learning criteria. Inclusion of absorptive soffit expected to reduce exceedance to within compliant levels for majority of the COLA.
Outdoor learning centre for Support learning unit (OLC for SLU)	38-51	Yes	Within target criteria for outdoor teaching and learning. 1 dB exceedance considered negligible.

All feasible and reasonable mitigation measures have been implemented to reduce partial non-compliances. Residual exceedances are minimal and considered acceptable on the basis of conservative assessment parameters representing worst case scenario.

## 4. Construction noise and vibration assessment

#### 4.1 Construction noise

#### 4.1.1 Construction activities

The construction phases used as the basis of this assessment are summarised below and has been based on reference schools such as Melonba High School. The overall programme for these works is anticipated to be 17 months.

- Site establishment
- Excavation / Earthworks
- Substructure
- Structural / Concreting
- Building envelope
- Fitout / Finishes
- External works / Landscaping
- Demobilisation

Assumed construction equipment to be used for redevelopment works are provided in Table 37.

Equipment sound power levels have been determined by reference to AS2436, BS5228, and Arup's measurement database. The equipment below has been assumed to operate concurrently however equipment sound power levels have been adjusted according to its usage in a worst case 15-minute period, and penalty corrections for impulsive noise characteristics.

The locations of equipment have been based on the locations of the construction works around the precinct.

Table 37: Construction equipment usage and associated sound power levels (Lw)

Plant item	Plant item sound power level, dBL <sub>Aeq</sub>	Penalty, dB	% of use in worst case 15 mins	Site Establishment	Excavation / Earthworks	Substructure	Structural / concreting	Building Envelope	Fitout & finishes	External works / landscaping	Demobilisation
Truck (>20 Tonne)	107	0	50	1	1	1	1	1	1		1
Crane (Mobile)	113	0	50				1		1		1
Loader (Front-end) (23t)	112	0	50	1	1						1
Generator (Diesel)	113	0	100	1			1		1		
Excavator (10t)	100	0	50		1						
Excavator (10t) + hydraulic hammer	118	5	50		1						
Loader - Skidsteer (Bob-cat) (1/2t)	107	0	50		1					1	
Truck (Dump)	117	0	50		1						
Piling (Bored)	111	0	10			1					
Concrete Pencil Vibrator	105	0	10			1	1				
Concrete Pump	109	0	25			1	1				
Hand Tools (Electric)	110	0	50				1	1	1	1	1
Road Lorry (Full)	108	0	50		1			1			
Concrete Agitator Truck	111	0	50			1	1				
Scissor lift	98	0	50				1	1	1		
Angle Grinder	108	0	25					1			
Welder	110	0	25						1		
Forklift	106	0	50							1	
Crane (Truck Mounted)	108	0	50	1			1	1			

#### 4.1.2 Assessment methodology

Noise emissions from construction activities have been assessed to criteria outlined in Section 2.5.2.

Noise emissions have been modelled using SoundPLAN 9 in accordance with ISO9613-2 algorithms. The model included:

- Construction noise sources listed in Section 4.1.1;
- Surrounding buildings, ground terrain and absorption; and
- Receivers listed in Section 1.1.

Noise emissions have been modelled on the following assumptions:

- Equipment, staging and durations are based on typical scenarios for NSW school projects.
- Construction areas have been derived based on the latest architectural site plans.
- The location of equipment will be spread evenly across the site.

#### 4.1.3 Noise prediction results

Predicted construction noise levels at surrounding noise sensitive receivers along with the relevant NML for the intended working hours are presented in Table 38.

**Table 38: Predicted construction noise levels** 

Receiver ID	Classification	NML	Construction Phase							
			Site Establishment	Excavation / Earthworks	Substructure	Structural / Concreting	Building Envelope	Fit out & finishes	External work / landscaping	Demobilisation
R1	Residential	51	69	70	65	71	66	70	64	68
R2	Residential	51	50	51	46	52	47	51	45	49
R3	Residential	51	49	50	41	47	42	46	44	48
R4	Residential	51	47	48	41	47	42	46	42	46
R5	Residential	51	50	51	45	51	46	50	45	49
R6	Residential	51	51	52	47	53	48	52	46	50
R7	Residential	51	53	54	49	55	50	54	48	52
R8	Residential	51	55	56	52	58	53	57	50	54
R9	Residential	51	52	53	49	55	50	54	47	51
R10	Residential	51	48	49	45	51	46	50	43	47
R11	Residential	51	60	61	52	58	53	57	55	59
R12	Residential	51	47	48	41	47	42	46	42	46
R13	Residential	51	46	47	41	47	42	46	41	45
R14	Residential	51	46	47	42	48	43	47	41	45

Receiver ID	Classification	NML	Construction Phase							
			Site Establishment	Excavation / Earthworks	Substructure	Structural / Concreting	Building Envelope	Fit out & finishes	External work / landscaping	Demobilisation
R15	Residential	51	45	46	42	48	43	47	40	44
R16	Residential	51	61	62	58	64	59	63	56	60
S1	School	55 <sup>1</sup>	58	59	52	58	53	57	53	57
H1	Healthcare	55 <sup>1</sup>	62	63	60	66	61	65	57	61
I1	Industrial	75	65	66	63	69	64	68	60	64
I2	Industrial	75	65	66	62	68	63	67	60	64
13	Industrial	75	64	65	61	67	62	66	59	63
I4	Industrial	75	61	62	57	63	58	62	56	60
15	Industrial	75	59	60	55	61	56	60	54	58
I6	Industrial	75	58	59	54	60	55	59	53	57
I7	Industrial	75	54	55	50	56	51	55	49	53
18	Industrial	75	53	54	49	55	50	54	48	52
C1	Commercial	70	64	65	56	62	57	61	59	63
C2	Commercial	70	56	57	54	60	55	59	51	55
С3	Commercial	70	63	64	59	65	60	64	58	62

#### Notes:

Levels shaded in grey indicate a notional exceedance of NMLs based on the worst-case assumptions noted above.

Levels in **BOLD RED** represent 'highly affected' noise levels of 75dBA or above.

 $1-10~\mathrm{dB}$  is added to the façade incident sound pressure level result to account for the criteria for schools and hospitals being an internal noise criteria

Results indicate that residential receivers to the north of site (R1, R16, R11), and south of site (R7, R8) are worst affected due to proximity. These receivers are predicted to experience NML exceedances of up to 20 dB during worst case scenarios.

Results indicate comparable levels to the nearest affected non-residential receivers, with the exception of industrial and commercial receivers. Exceedances of up to 11 dB during the anticipated worst case periods are predicted at H1, the medical centre, and up to 4 dB at S1, the primary school.

During construction, plant and equipment will move through the Project area as the Project progresses, changing noise impacts in relation to the nearby individual sensitive receivers. The noise levels experienced at a particular location will rise and fall in accordance with the varying offset distance of the works, the intensity and location of construction activities, the intervening terrain and structure and the type of equipment used. It is unlikely that all construction equipment will be operating at their maximum sound levels simultaneously. In any given period, typically construction equipment would be used with maximum

sound levels for only a brief amount of time and at other times the equipment may emit lower sound levels carrying out activities.

In general, construction works are temporary in nature therefore potential noise impact on the community and the surrounding environment will not be permanent or continuous. Where the predicted LAeq(15min) noise level is greater than the noise management levels all feasible and reasonable work practices should be applied, as recommended below.

#### 4.1.4 Construction noise mitigation and management measures

Indicative noise reduction for different noise mitigation measures relevant to construction activities for the project have been obtained from the guidance of AS2436 - Guide to Noise and Vibration Control on Construction, Demolition and Maintenance Sites and BS5228.1 - Code of Practice for Noise and Vibration Control on Construction and Open Sites - Noise, and are summarised below in Table 22 for reference.

Table 39: Indicative noise reduction provided by noise mitigation measures

Construction equipment	Noise mitigation measure	Indicative noise reduction	Source
Jackhammer	Muffler and screen	20 dBA	Table C2, AS2436:2010
Compressor, Cement mixers, Hand-held tools	Screening	5 dBA	Table C3, AS2436:2010
Excavators/loaders, Trucks, Mobile cranes, Asphalt paver, Bulldozers, Road graders, Rollers/compactors	Residential-grade silencer	10 dBA	Table C2, AS2436:2010 Table B1, BS5228.1:2009
Excavator with hammer attachment	Residential-grade silencer, Screening of hammer attachment	15 dBA	Table C2, AS2436:2010
Piling impact	Resilient pad (dolly) between pile and hammerhead	10 dBA	Table C2, AS2436:2010 Table B1, BS5228.1:2009

Table 40 provides a summary of the potential project specific community consultation measures depending on the extent of NML exceedances. This table has been informed by the Construction Noise and Vibration Strategy (CNVS) and should be reviewed and refined for the development of the Construction Noise and Vibration Management Plan (CNVMP) for the project to be developed by the contractor.

Table 40: Indicative community consultation measures

Construction hours	Receiver perception	Above NML	Management Measures <sup>1,2,3,4</sup>
Airborne noise			
Standard hours (day)	Noticeable	≤ NML (compliant	-
	Clearly audible	≤ NML + 10	-
	Moderately intrusive	≤ NML + 20	N
	Highly intrusive	> NML + 20	N
	Highly noise affected	≥ 75 dBA	N, SN, RP
Outside standard hours	Noticeable	≤ NML (compliant	-
(night) <sup>5</sup>	Clearly audible	≤ NML + 10	N
	Moderately intrusive	≤ NML + 20	N, SN

Construction hours	Receiver perception	Above NML	Management Measures <sup>1,2,3,4</sup>
	Highly intrusive	> NML + 20	N, SN, AA, RP
	Highly noise affected	≥75 dBA	N, SN, AA, RP

#### Notes:

- 1. N: Notifications (such as letter box drops)
- 2. SN: Specific notifications such as individual briefings or phone call
- 3. AA: Alternative accommodation
- 4. RP: Respite Period
- 5. No works outside of standard hours is proposed. Management measures are for information only.

#### 4.2 Construction traffic

Construction-related road traffic is a temporary source of noise that must be assessed and managed, particularly concerning heavy vehicles accessing the site. To minimise disturbance to the neighbouring community, truck arrivals and departures should be scheduled outside peak traffic hours and, wherever possible, during times that are less sensitive to noise.

Details of predicted construction traffic volumes are not available at this early stage of design. The increase in traffic caused by construction is expected to be minimal, with the total number of vehicles rising by less than 60% compared to existing traffic. This increase will result in a noise level rise of under 2 dB, which is below the threshold for traffic noise increase screening criteria as discussed in Section 2.3.3.

It is important to acknowledge, however, that heavy vehicles can produce noise levels higher than regular car traffic, leading to more significant disturbances. To mitigate this, access routes should be limited to major roads and avoid local residential streets as far as practicable. Measures such as avoiding engine braking, adhering strictly to speed limits, and minimising sudden braking or acceleration should also be enforced.

All contractors and subcontractors should be informed about the importance of noise-conscious driving when traveling to and from the construction site. To manage noise from construction traffic, the following measures should be implemented:

- Staging truck arrivals to prevent queuing and idling on public streets.
- Directing vehicles to arrive and depart via designated routes that minimize the use of local roads.
- Reducing the need for reversing to limit the use of reversing alarms ("beepers") and/or using quieter alarms (e.g., quacker alarms).
- Minimising engine braking and avoiding unnecessary noise from slamming doors, loud radios, shouting, or the use of truck horns for signalling.

The contractor will also need to evaluate cumulative noise impacts as part of the Construction Noise and Vibration Management Plan (CNVMP). Coordination with other contractors and projects in the area will be necessary if construction activities occur simultaneously.

#### 4.3 Vibration

As a guide, the recommended minimum working distances for vibration intensive plant in Table 41 (which has been derived from the TfNSW CNVS) provide an indication of the possibility of impact due to vibration generating plant and equipment onto nearby receivers. While the minimum working distances are indicative only and will vary depending on the item of plant and local geotechnical conditions, if a receiver is located within the minimum working distance, vibration monitoring might be required, and equipment selection and/or method of construction might have to be reviewed.

Table 41: Recommended minimum working distances (m) for vibration generating plant

Plant item	Rating / description	Minimum working distance (m)					
	uescription	Cosmetic damage	Human response				
		Industrial and heavy commercial buildings BS 7385 Line 1 -25 mm/s (See note 2)	Residential and light commercial buildings BS 7385 Line 2 - 7.5 mm/s (See note 2)	Structures unsound DIN 4150 Line 3 – 3 mm/s	response		
Vibratory roller	< 50 kN (~ 1 to 2t)	2 m	5 m	11 m	15 m to 20 m		
	< 100 kN (~ 2 to 4t)	2 m	6 m	13 m	20 m		
	< 200 kN (~ 4 to 6t)	5 m	12 m	26 m	40 m		
	< 300 kN (~ 7 to 13t)	6 m	15 m	31 m	100 m		
	> 300 kN (~ 13 to 18t)	8 m	20 m	40 m	100 m		
	> 300 kN (> 18t)	10 m	25 m	50 m	100 m		
Hydraulic hammer  – Small	300 kg / 5 to 12t excavator	1 m	2 m	5 m	7 m		
Hydraulic hammer  – Medium	900 kg / 12 to 18t excavator	3 m	7 m	15 m	23 m		
Hydraulic hammer  – Large	1600 kg / 18 to 34t excavator	9 m	22 m	44 m	73 m		
Piling – Vibratory	Sheet piles	9 m	22 m	44 m	73 m		
Piling - Bored	≤ 800 mm	1 m (nominal)	2 m	5 m	10 m		
Piling – Hammer	12t down force	6 m	15 m	30 m	50 m		
Jackhammer	Hand-held	1 m (nominal)	1 m (nominal)	3 m	5 m		
Mechanised bored tunnelling works (Tunnel Boring Machine, Horizontal Directional Drilling, Micro- tunnelling)1	-	1 m to 5 m	2 m to 12 m	4 m to 24 m	6 m to 35 m		

#### Note:

The safe working distances presented are indicative and will vary depending on the particular item of plant and local geotechnical conditions. They apply to cosmetic damage of typical buildings under typical geotechnical conditions.

<sup>1</sup>\_Based on TRL document using Godio et al formula, equation 24

<sup>2</sup>\_Where vibration might give rise to resonant responses in structures

The contractor will be required to manage vibration as well as noise and make use of best practice in the management of vibration using simple and practicable techniques such as avoiding dropping heavy items.

Where vibration intensive works are required within the minimum working distances outlined in Table 41, vibration monitoring at the nearest potential affected building should be considered, where real-time alerts can be generated when measured vibration levels exceed criteria.

## 5. Conclusion

An acoustic assessment has been undertaken of construction and operation of the proposed New High School for Medowie. This assessment has been based on information available at this stage of design and has been developed to a level of detail suitable for submission as appendix to the Review of Environmental Factors.

The operational assessment has considered noise emissions from school operations including building services, outdoor play areas, gymnasium use, outdoor workshop areas and car parks. Road traffic noise increase associated with operation of the school has also been assessed along with noise intrusion into the development site. Various recommendations have been made to mitigate noise sources and enhance the building envelope where feasible and reasonable to demonstrate compliance with target criteria.

In lieu of detailed information being available at this stage of design, the construction noise and vibration assessment has made various assumptions based on typical approaches to building school developments. Various exceedances of target noise management levels have been identified and indicative mitigation and management measures put forward. A detailed Construction Noise and Vibration Management Plan will be required to be developed by the Contractor once more specific details are known.

Assessment of acoustic impact has been compared against relevant environmental criteria. Accompanying mitigation and management measures are proposed to effectively address any identified exceedances of screening criteria. On the basis of this assessment, the proposed activity is not expected to have a significant acoustic impact on the environment.

## 6. Mitigation Measures

**Table 42: Mitigation measures** 

Mitigation Name	Section	Mitigation Measure	Reason for Mitigation Measure
Building services	Section 3.2	Appropriate equipment selection and noise mitigation design.	Achieve internal and external building services noise and vibration criteria.
Operational activities	Section 3.3	Acoustic louvres to be installed within Gymnasium and Covered Outdoor workshop areas where required to achieve environmental noise emission criteria.	To minimise disruption to nearby residential receivers.
		Implement feasible and reasonable mitigation measures for traffic generation in alignment with the NSW Road Noise Policy.	
		Restrict usage of Public Address to daytime hours only (7am to 6pm). Use directional speakers and set volume levels to the minimum required to ensure clarity and audibility.	
		Where practicable, all loading dock activities, waste removal and noisy cleaning activities should take place between 7:00 AM and 10:00 PM.	
Noise intrusion	Section 3.4	Façade glazing and lightweight elements and doors to be designed to control noise break-in to sensitive areas.	To control noise intrusion into sensitive spaces throughout the school.
		Natural ventilation to incorporate acoustic louvres where noise break-in is required to be controlled.	
		Install acoustically absorptive finishes to underside of outdoor learning areas to control reverberation build up and mitigate noise intrusion.	
Construction noise and vibration	Section 4	Contractor to develop a detailed construction noise and vibration management plan once specific details of proposed construction activities and staging are known.	To effectively manage construction noise and vibration impacts to the surrounding community.

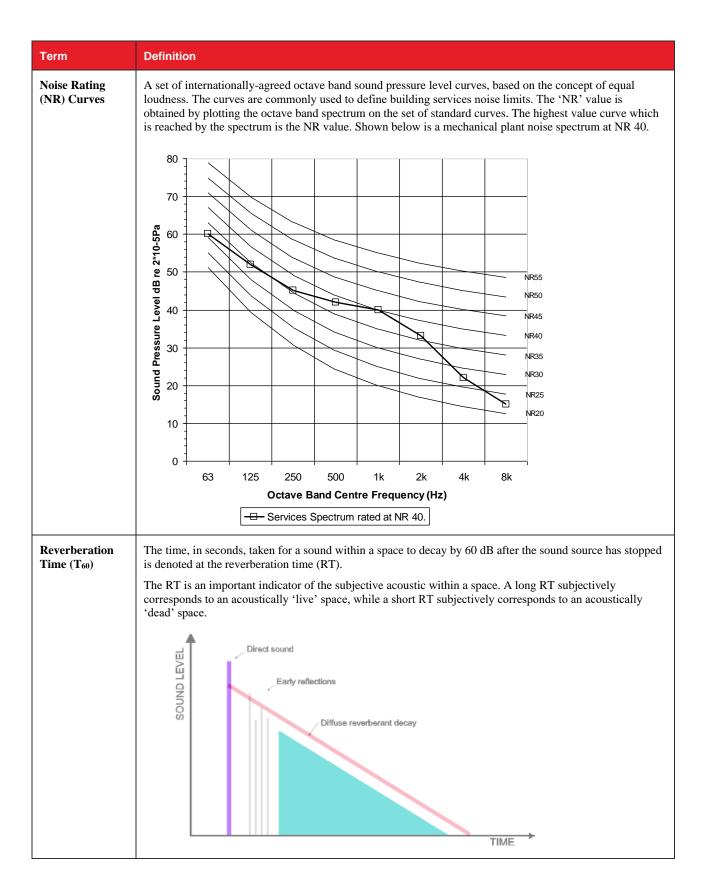
# Appendix A

**Glossary** 

Term	Definition
Absorption Coefficient, α	The amount of sound absorbed by a material, defined as the ratio of the amount of acoustic absorption of the material (in units of sabins) to the material's surface area. Absorption coefficient is broadly equivalent to the proportion of sound energy absorbed by the material.
	Noise-reduction Coefficient (NRC): The arithmetic average of the sound-absorption coefficients of a material at 250 Hz, 500 Hz, 1 kHz and 2 kHz. It is a simplified single-number index that provides an indication of the sound absorbing efficiency of a material, typically ranging from 0 to 1. The rating is affected by type, thickness, density and mounting of the material.
	Weighted absorption coefficient ( $\alpha_w$ ): The weighted absorption coefficient, defined in ISO 11654 is a frequency-weighted single number absorption coefficient used to categorise the overall absorption effectiveness of a material.
	Descriptors are used to indicate if the material absorbs strongly at high (H), mid (M) and/or low (L) frequencies – e.g. a material may be rated as $\alpha_w 0.85(LH)$ , which indicates that it strongly absorbs at both low and high frequencies.
	Materials can also be assigned into five absorption classes, with Class A having the highest absorption and Class E having the lowest absorption.
Ambient noise level	The ambient noise level is the overall noise level measured at a location from multiple noise sources. When assessing noise from a particular development, the ambient noise level is defined as the remaining noise level in the absence of the specific noise source being investigated. For example, if a fan located on a building is being investigated, the ambient noise level is the noise level from all other sources without the fan operating, such as traffic, birds, people talking and other noise from other buildings.
Background noise level	The background noise level is the noise level that is generally present at a location at all or most times. Although the background noise may change over the course of a day, over shorter time periods (e.g. 15 minutes) the background noise is almost-constant. Examples of background noise sources include steady traffic (e.g. motorways or arterial roads), constant mechanical or electrical plant and some natural noise sources such as wind, foliage, water and insects.
	Assessment Background Level (ABL): A single-number figure used to characterise the background noise levels from a single day of a noise survey. ABL is derived from the measured noise levels for the day, evening or night time period of a single day of background measurements. The ABL is calculated to be the tenth percentile of the background $L_{A90}$ noise levels – i.e. the measured background noise is above the ABL 90% of the time.
	Rating Background Level (RBL / minLA90,1hour): A single-number figure used to characterise the background noise levels from a complete noise survey. The RBL for a day, evening or night time period for the overall survey is calculated from the individual Assessment Background Levels (ABL) for each day of the measurement period, and is numerically equal to the median (middle value) of the ABL values for the days in the noise survey.
Decibel (dB)	The logarithmic scale used to measure sound and vibration.
	Human hearing is not linear and involves hearing over a large range of sound pressures, which would be challenging to present on a linear scale. A logarithmic scale allows all sound levels to be expressed based on how loud they are relative to a reference sound (typically 20 $\mu$ Pa, which is the approximate human threshold of hearing). For sound in other media (e.g. underwater noise) a different reference level (1 $\mu$ Pa) is used instead.
	An increase of approximately 10 dB corresponds to a subjective doubling of the loudness of a noise. The minimum increase or decrease in noise level that can be noticed is typically 2 to 3 dB.

Term	Definition
dB weighting curves	The frequency of a sound affects its perceived loudness and human hearing is less sensitive at low and very high frequencies. When seeking to represent the summation of sound pressure levels across the frequency range of human hearing into a single number, weighting is typically applied. Most commonly, A-weighting, denoted as dB(A), is used for environmental noise assessment. This is often supplemented by the linear or C-weighting curves, where there is the potential for excess low-frequency sound at higher sound pressure levels.  10  0  dB(C)  dB(A)  30  40
	్రం బ్యాంక్ మ్ చి
dB(A)	dB(A) denotes a single-number sound pressure level that includes a frequency weighting ('A-weighting') to reflect the subjective loudness of the sound level.
	The frequency of a sound affects its perceived loudness. Human hearing is less sensitive at low and very high frequencies, and so the A-weighting is used to account for this effect. An A-weighted decibel level is written as dB(A).
Flutter Echo	Flutter echo refers to an acoustic defect where sound reflects backwards-and-forwards between a set of parallel surfaces with very little energy loss. The resulting flutter echo decays very slowly and can 'linger' in the room long after sound travelling in other directions has been attenuated.
	Flutter echo can cause distortion to the sound quality, making it sound 'metallic', or if the flutter is strong enough or delayed enough, it can cause a sound to be 'blurred' and even be heard as a separate sound (a true 'echo').
	Flutter is treated by angling surfaces so they are not parallel (typically a minimum of 7° off-parallel), adding absorption to one or both surfaces, or by adding diffusion to one or both surfaces.

Term	Definition				
Frequency	Frequency is the number of cycles per second of a sound or vibration wave. In musical terms, frequency is described as 'pitch'. Sounds towards the lower end of the human hearing frequency range are perceived as "bass" or 'low-pitched' and sounds with a higher frequency are perceived as 'treble' or 'high pitched'.				
	The unit of frequency is the hertz (Hz), which is identical to cycles per second. A thousand Hz is generally denoted as kHz. Human hearing ranges approximately from 20 Hz to 20 kHz.				
	While single weighted sound pressure levels simplify the assessment and evaluation of sound levels, frequency analysis is often undertaken. 'Octave bands', either 1/1 or 1/3 octave bands are most commonly utilised and are referred to by the nominal centre frequency of the band (e.g. 31.5 Hz), while being the summation of all frequencies between a defined lower and upper frequency.				
	110				
	100 — 63 — 125 — 250 — 250 — 31.5 — 3				
	1/3 Octave Band Centre Frequency (Hz)				
Impact Sound	The technical parameter used to determine impact sound isolation of floors is the impact sound pressure				
Pressure Level	The technical parameter used to determine impact sound isolation of floors is the impact sound pressure level, L <sub>i</sub> .  In the laboratory, the weighted normalised impact sound pressure level, L <sub>n,w</sub> , is used to represent the impact sound isolation as a single figure.  On site, the weighted normalised apparent impact sound pressure level, L' <sub>n,w</sub> , and the weighted standardised apparent impact sound pressure level, L' <sub>n,Tw</sub> , are used to represent the impact sound isolation of a floor as a single figure.  These single weighted values are determined by comparing the spectral impact sound pressure levels (as defined in ISO 140-6 and ISO 140-7) with reference values outlined in AS/NZS ISO 717.2.				
L <sub>10</sub> (period)	The sound level exceeded for 10% of the measurement period, or alternatively, the sound levels would be lower for 90% of the time.				
	The $L_{10}$ is often defined as the 'average maximum' sound levels, as in AS1055-2018 with the advent of statistical sound level meters.				
L90(period)	The sound level exceeded for 90% of the measurement period.  The L <sub>90</sub> is often defined as the 'average minimum' or 'background' noise level for a period of measurement. For example, 45 dBL <sub>A90,15min</sub> indicates that the sound level is higher than 45 dB(A) for 90% of the 15-minute measurement period.				
Leq(period)	The equivalent ('eq') continuous sound level, used to describe the level of a time-varying sound or vibration measurement.				
	The L <sub>eq</sub> is often defined as the 'average' level, and mathematically, is the energy-average level over a measurement period – i.e. the level of a constant sound that contains the same sound energy as the measured sound.				
L <sub>peak</sub> / L <sub>max</sub>	The $L_{peak}$ is the 'absolute maximum' level of a sound or vibration recorded within the measurement period. As the $L_{peak}$ is often caused by an instantaneous event, it can vary significantly between measurements.				
	$L_{max}$ is the maximum rms sound pressure level within a measuring period. $L_{max}$ gives a better picture of what the general maximum level was in a measurement, making it easier to calculate and measure for a noise source waveform that is changing constantly in its magnitude.				

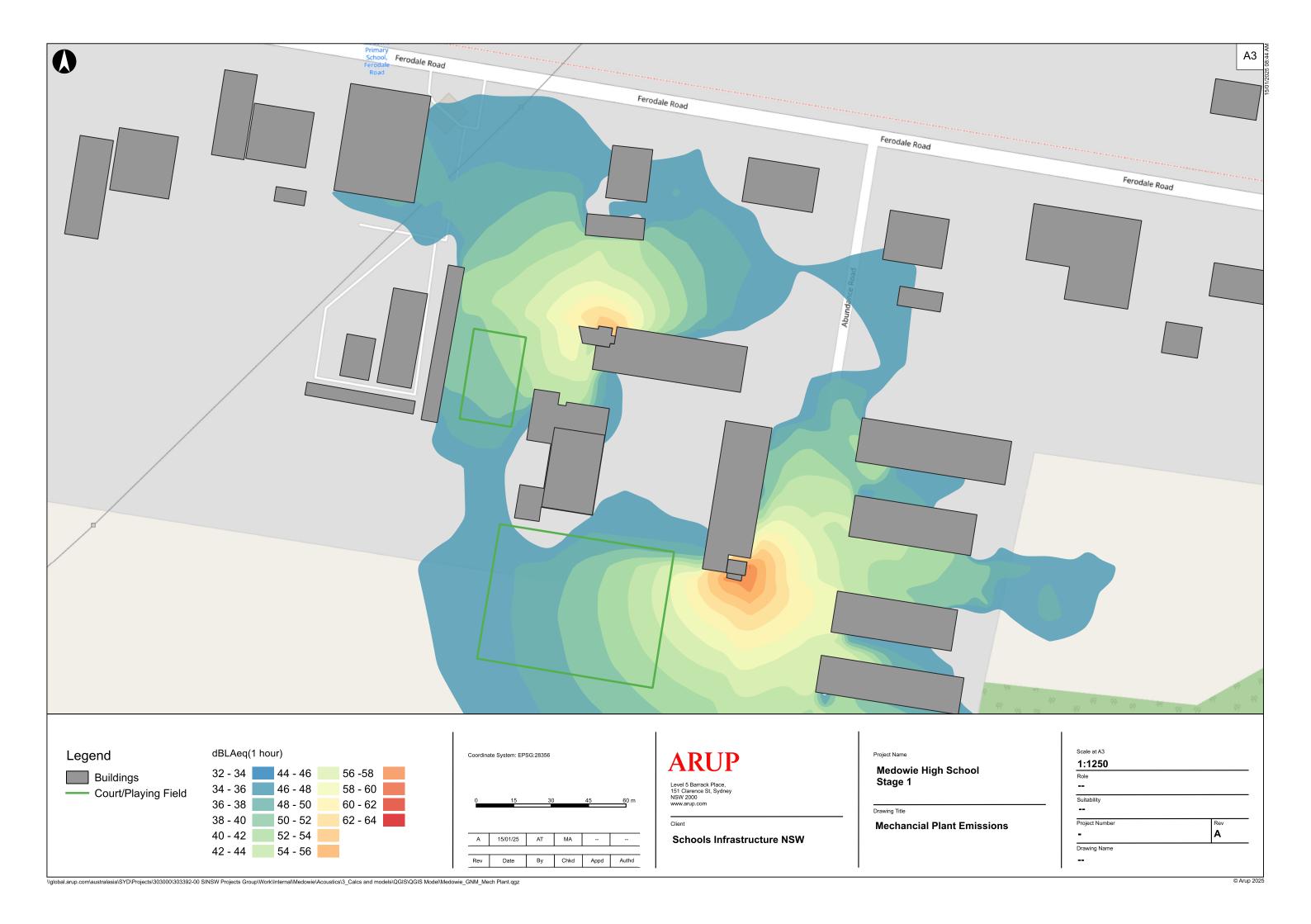


Term	Definition						
Sound Level Difference (D)	Used to quantify the sound insulation between two spaces and is equal to the difference in sound level between the rooms within a particular frequency band. For example, if the sound level in the source room is 100 dB and the sound level in the adjacent room is 75 dB, the sound level difference is 25 dB for that frequency band.						
	The weighted sound level difference, $D_w$ , as defined in AS/NZS ISO 717.1, is used to provide a single-number descriptor to describe the overall performance of a partition across multiple frequency bands. Note however that $D_w$ is only calculated over a frequency range from 100 Hz to 3.15 kHz and hence sound outside of this range is excluded from calculation of $D_w$ – particularly low frequency (bass) sound below 100 Hz.						
	Also used are the weighted normalised level difference $(D_{n,w})$ , which corrects the measured sound level difference to a reference sound absorption area in the receiving room, or the weighted standardised level difference $(D_{nT,w})$ , which corrects the measurements to a reference reverberation time in the receiving room.						
	These single numbers are determined by comparing the spectral sound insulation test results (as defined in ISO 140-4) with reference values, as outlined in AS/NZS ISO 717.1.						
Sound Power and Sound Pressure	The sound power level $(L_w)$ of a source is a measure of the total acoustic power radiated by a source. The sound pressure level $(L_p)$ varies as a function of the environment and distance from a source.						
Tressure	The sound power level is an intrinsic characteristic of a source (analogous to its mass), which is not affected by the environment within which the source is located.						
Sound Reduction Index (R)	A measure of the sound level loss through a material for a particular frequency band. Sound reduction index is sometimes also referred to as transmission loss. It is a property of the component, unlike the sound level difference, which is affected by the common area between the rooms and the acoustics of the receiving room. R is the ratio (expressed in decibels) of the sound energy transmitted through the building element to the sound energy incident on the building element for a particular frequency band.						
	The weighted sound reduction index, $R_w$ , is a single figure description of sound reduction index across multiple frequency bands and is defined in BS EN ISO 717-1: 2000. $R_w$ values are calculated from measurements in an acoustic laboratory. Note however that $R_w$ is only calculated over a frequency range from 100 Hz to 3.15 kHz and hence sound outside of this range is excluded from calculation of $R_w$ – particularly low frequency (bass) sound below 100 Hz.						
	Sound insulation ratings derived from site measurements are referred to as apparent sound reduction index (R'w) ratings.						
Spectrum Adaptation Terms (C and Ctr)	$C$ and $C_{tr}$ denote a spectrum adaptation (in dB) that are added to the $R_w$ or $D_w$ value of a partition to adjust for different sound characteristics.						
	C is used to measure the performance of a partition for medium to high-frequency sound sources, such as speech.						
	C <sub>tr</sub> is used to measure the performance of a partition for low-frequency sound sources such as road traffic.						
	The values of C and $C_{tr}$ are dependent on the construction of the partition and are usually negative quantities, they typically increase the $R_w$ requirement of a partition. For example, for a partition with an $R_w$ of 56 dB and $C_{tr}$ -6 dB, the $R_w$ + $C_{tr}$ is only 50 dB.						
	The overall performance of the partition is quoted as the sum of the $R_w$ value and the spectrum adaptation terms, e.g. $D_w+C$ 55 dB; $R_w+C_{tr}$ 60 dB.						

Term	Definition							
Speech Transmission Index (STI)	STI is a technical index, predictable and measurable using specialised equipment, for assessing speech and vocal intelligibility. STI takes into account the signal/noise ratio of the speech signal and the reverberation of the receiving environment. The higher the value of STI, the higher the expected speech intelligibility.  STI ratings are assigned subjective categories, as follows:							
		STI range	Subjective category					
		< 0.3	Bad					
		0.3 - 0.45	Poor					
		0.45 - 0.6	Fair					
		0.6 - 0.75	Good					
		0.8 – 1.0	Excellent					
Structureborne noise	The transmission of noise energy as vibration of building elements. The energy may then be re-radiated as airborne noise. Structureborne noise is controlled by structural discontinuities, i.e. expansion joints and floating floors.							
Vibration	Waves in a solid material are called 'vibration', as opposed to similar waves in air, which are called 'sound' or 'noise'. If vibration levels are high enough, they can be felt; usually vibration levels must be much higher to cause structural damage.							
	A vibrating structure (e.g. a wall) can cause airborne noise to be radiated, even if the vibration itself is too low to be felt. Structureborne vibration limits are sometimes set to control the noise level in a space.  Vibration levels can be described using measurements of displacement, velocity and acceleration. Velocity and acceleration are commonly used for structureborne noise and human comfort. Vibration is described using either metric units (such as mm, mm/s and mm/s²) or else using a decibel scale.							

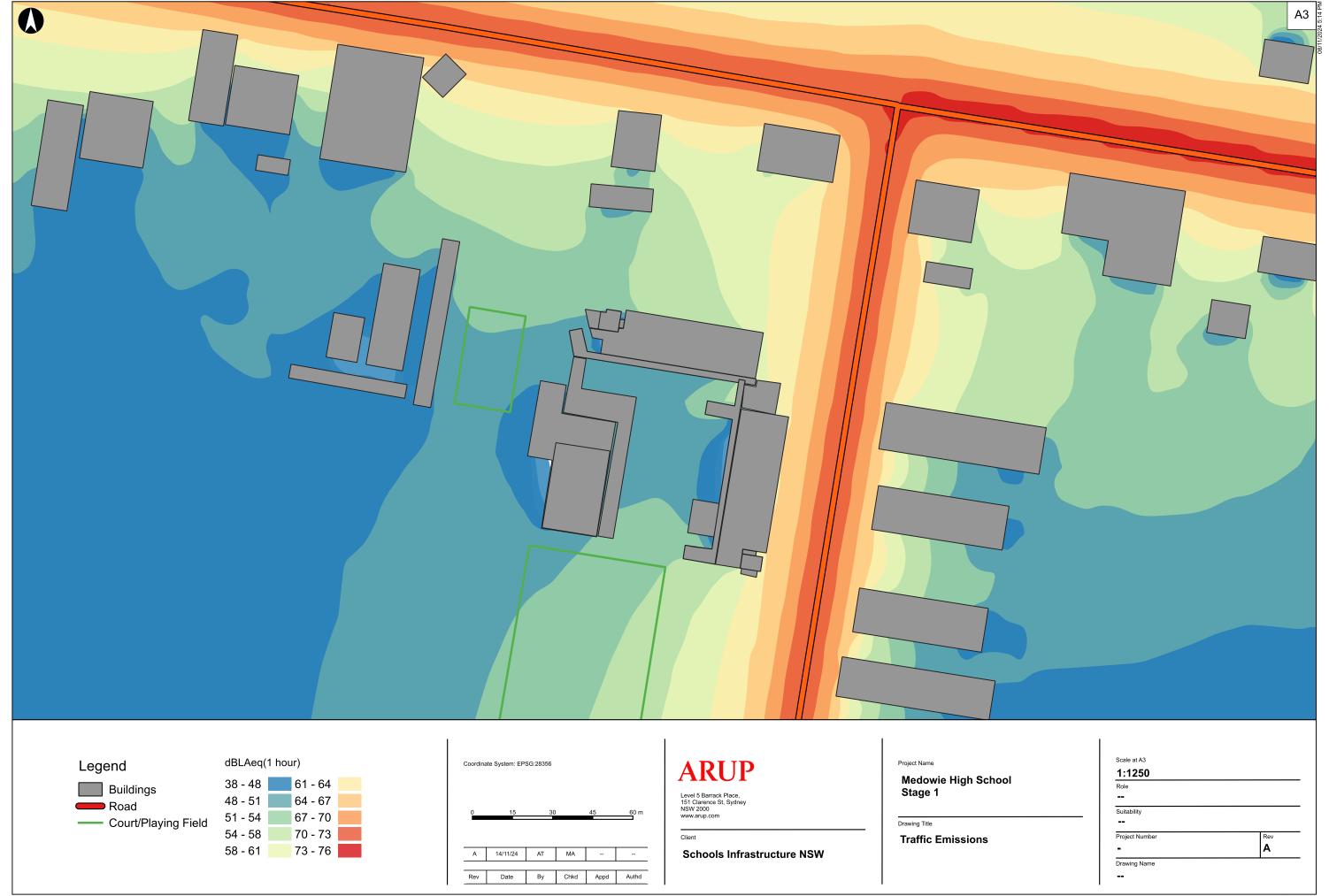
# Appendix B

**Mechanical plant noise** 



# Appendix C

Road traffic noise



# Appendix D REF Checklist

Requirement	Υ	N	N/A	Comments
			.471	Comments
Noise and vibration				<b>—</b>
Noise monitoring				This report
Does the REF include an Noise and Vibration				
Impact Assessment (NVIA)?				Continu 4.2
Does the assessment include background noise				Section 1.3
monitoring at locations that appropriately represent				
the existing noise levels at nearby sensitive				
receivers (i.e. residences, churches, health				
facilities, etc.)?		П		Section 1.3
Does the background noise monitoring undertaken meet the requirements of Noise Policy for Industry		ш	Ш	Section 1.5
(2017) i.e. at least a week with acceptable weather				
conditions:				
average wind speed <5 m/s?				
<ul> <li>no rain or other extraneous noise?</li> </ul>				
Construction noise	$\square$	П	П	Section 4.1
Does the assessment consider impacts from				Section 4.1
construction noise and vibration in accordance with				
the Interim Construction Noise Guideline?				
Does it:	$\boxtimes$			Section 2.5.2
determine noise management levels for the				33011011 2.3.2
development?				
predict noise levels of the proposed	$\boxtimes$		П	Section 4.1.3
construction activities (usually of expected				- Coulon 1.1.6
standard activities and equipment and				
associated noise levels given that full				
construction methodology will not yet be				
known)?				
conclude whether the predicted levels would	$\square$	П	П	Section 4.1.3
exceed the noise management levels?				
set out measures to minimise impacts to	$\square$	П	П	Section 4.1.4
sensitive receivers, including existing school				
users, and ensure best practice on site?				
conclude whether construction noise would be	$\square$			Section 4.1.3
likely to result in significant impacts?				
adopt standard construction hours set out in	$\boxtimes$		П	Section 2.5.1
the ICNG or include justification where non-				
standard hours are proposed?				
Vibration	$\boxtimes$			Section 2.5.3
Does the assessment include an assessment of				
potential impacts as a result of vibration during				
constriction which:				
<ul> <li>relevant standards and assessment criteria for</li> </ul>				
human comfort, sensitive equipment and				
structural damage?				
details potential sources of vibration during	$\boxtimes$			Section 4.3
construction having regard to typical activities				
and equipment expected to undertake				
proposed construction works?				
consider potential impacts having regard to	$\boxtimes$			Section 4.3
separation distances to nearby sensitive				
receivers?				
sets out measures to mitigate potential	$\boxtimes$			Section 6
impacts, including existing school users?				
concludes that the proposed activity would not	$\boxtimes$			Section 4.3
be likely to have significant environmental				
affects following mitigation?				
Operational noise	$\boxtimes$			Section 2.3
-	t .	1		1

Requirement	Υ	N	N/A	Comments
Does the assessment:				
<ul> <li>consider noise impacts from all aspects of</li> </ul>				
proposed operations in accordance with the				
Noise Policy for Industry (2017) or Association				
of Australasian Acoustical Consultants				
Guideline for Child Care Centre Acoustic				
Assessment in the case of outdoor play?	$\boxtimes$			
determine noise criteria that would be				Section 2
applicable?			П	Section 3.3
<ul> <li>consider all proposed activities, including:</li> <li>indoor learning activities?</li> </ul>	$\boxtimes$			Section 3.3
o outdoor play?	$\boxtimes$			Section 3.3.1
use of public address system?				Section 3.3.6
<ul> <li>plant and equipment (i.e. air conditioning)</li> </ul>				Section 3.2
use of the hall	$\boxtimes$			Section 3.3.2
use of outdoor sports courts				Section 3.3.1
conclude that the proposal would meet the				Section 3
project noise trigger levels?				Geotion o
set out mitigation measures if the proposal	$\boxtimes$			Section 6
does not meet the trigger levels, does the				
assessment				
Internal noise tenability				Section 3.4
Does the assessment:				
consider external sources of noise in proximity     to the site (i.e. main reads or reil corridors)?				
to the site (i.e. main roads or rail corridors)?				Section 2.4.1
<ul> <li>detail applicable internal noise comfort criteria having regard to the EFSG?</li> </ul>				Occilor 2.4.1
predict internal noise levels?	$\boxtimes$			Section 3.4
conclude that internal noise levels would meet	$\boxtimes$			Section 3.4
criteria?				
set out any proposed mitigation measures	$\boxtimes$			Section 6
required to meet the criteria?	$\boxtimes$			_
Overall assessment				Section 6
Does the assessment:				
<ul> <li>include a list of measures to mitigate the impacts of the activity?</li> </ul>				
conclude overall, that the activity would not be	$\boxtimes$		П	Section 5
likely to result in significant environmental		ш		Coston o
affects?				
Does the REF list any mitigation measures				Section 6
identified in the assessment and incorporate them				
into the design where applicable (i.e. does the				
design include mechanical ventilation where this is				
required to achieve internal comfort levels)?				